# INUINIC|IPAL PVC PRESSURE PUPE \& FITTIINGS 

## Blue Brute Pipe

## $4^{\prime \prime}-12^{\prime \prime}(100 \mathrm{~mm}-300 \mathrm{~mm})$

Designed for municipal applications, Blue Bruteß systems deliver superior strength with corrosion resistant performance and the ability to flex without damage. IPEX municipal pressure piping systems are made with a high-strength, high-impact PVC compound, allowing them to perform even under high traffic loads and deep burial conditions.


## Corrosion-Proof Performance

IPEX Blue Brute systems are immune to corrosion from aggressive soils and galvanic action.

## Superior Hydraulics

The glass-like finish of PVC reduces friction losses and eliminates the tuberculation common in iron pipes. As a result, pumping costs are reduced and water quality is maintained.

## Cast Iron Outside Diameter (CIOD)

Blue Brute systems are manufactured with a cast iron outside diameter (CIOD). This is compatible with waterworks valves, appurtenances and restrainers.

Bottle-tight Joints, Removable Gaskets
IPEX's patented gasket system not only withstands many times the rated system pressure, but also withstands full vacuum pressures. The unique removable gasket system allows special oilresistant(nitrile) gaskets to be easily installed when working in contaminated soils.

## Third-party Certification

All IPEX municipal systems are third-party certified as applicable. In addition, IPEX Blue Brute systems have Factory Mutual approval and Underwriter's Laboratories (ULI and ULC) listings.

# Volume : <br> Pressure Piping Systems Design 

## Municipal Tedmical Mantul Series

Blue Brute ${ }^{\ominus}$ Piping Systems
IPEX Centurion ${ }^{\oplus}$ Piping Systems
CycleTough ${ }^{\oplus}$ Piping Systems
TerraBrute ${ }^{\oplus}$ Piping Systems
Q-Line ${ }^{\oplus}$ Water Service Tubing


# IPEX Pressure Piping Systems Design 

## Municipal Technical Manual Series

## Vol. 1, 2nd Edition

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The information contained here within is based on current information and product design at the time of publication and is subject to change without notification. IPEX does not guarantee or warranty the accuracy, suitability for particular applications, or results to be obtained therefrom.


## About IPEX

At IPEX, we have been manufacturing non-metallic pipe and fittings since 1951. We formulate our own compounds and maintain strict quality control during production. Our products are made available for customers thanks to a network of regional stocking locations throughout North America. We offer a wide variety of systems including complete lines of piping, fittings, valves and custom-fabricated items.

More importantly, we are committed to meeting our customers' needs. As a leader in the plastic piping industry, IPEX continually develops new products, modernizes manufacturing facilities and acquires innovative process technology. In addition, our staff take pride in their work, making available to customers their extensive thermoplastic knowledge and field experience. IPEX personnel are committed to improving the safety, reliability and performance of thermoplastic materials. We are involved in several standards committees and are members of and/or comply with the organizations listed on this page.

For specific details about any IPEX product, contact our customer service department (contact information is listed on the back cover).


## CONTENTS

Pressure Piping Systems Design Manual
About IPEX
Overview .....  1
Section One: Product Information
Introduction .....  3
Summary of Pressure Pipe and Fittings Testing .....  3
Blue Brute ${ }^{\circledR}$ Piping Systems .....  4
Applications .....  4
Gasket Options .....  5
Standards ..... 5
Short Form Specifications ..... 5
Dimensions ..... 6
IPEX Centurion ${ }^{\circledR}$ Piping Systems ..... 10
Applications ..... 10
Pressure Ratings ..... 11
Surge Pressures ..... 11
Gravity Applications ..... 12
Standards ..... 12
Short Form Specifications ..... 12
Dimensions ..... 13
CycleTough ${ }^{\circledR}$ Piping Systems ..... 14
Applications ..... 14
Pressure Ratings ..... 15
Standards ..... 15
Short Form Specifications ..... 15
Dimensions ..... 16
TerraBrute ${ }^{\circledR}$ Restrained Joint Pipe ..... 23
Applications ..... 23
Pulling Forces ..... 24
Bending Forces ..... 24
Standards ..... 26
Short Form Specifications ..... 26
Dimensions ..... 26
Q-Line ${ }^{\circledR}$ Water Service Tubing ..... 27
Applications ..... 27
Pressure Ratings ..... 28
Flow Rates ..... 28
Codes and Standards ..... 29
Short Form Specifications ..... 29
Dimensions ..... 29
Standards for PVC Pressure Systems ..... 30
Section Two: Properties of PVC Pressure Pipe and Pressure System Design Introduction ..... 31
Material Properties of PVC ..... 31
Design Life ..... 31
Design Strength ..... 32
Chemical Permeation and Installation of PVC Pipe in Contaminated Soils ..... 32
Thermal Effects and UV Resistance ..... 33
Expansion and Contraction ..... 33
Design Calculations
Calculating a Pressure Rating ..... 34
Calculating a Pressure Class ..... 34
Calculating Friction Headloss ..... 34
Calculating Surge Pressures ..... 35
Calculating Wave Velocity ..... 36
Air Entrapment in Pipelines ..... 36
Cyclic Fatigue in PVC Pipes ..... 38
Thrust Restraint in Gasketed Piping Systems ..... 38
Assembly, Installation and Testing of PVC Pressure Pipe Systems ..... 41
Section Three: Design Examples
Hydraulic and Cyclic Design Example ..... 43
Transmission Pipe Design Example ..... 46
Section Four: Appendices
Appendix A: References ..... 53
Appendix B: Reference Tables and Conversion Charts ..... 55
Appendix C: Useful Formulas ..... 60
Appendix D: Abbreviations ..... 62
Appendix E: Tables and Figures ..... 63

## Overview

IPEX Inc. is one of the largest manufacturers of plastic piping systems in North America. IPEX manufactures piping systems for many different applications, including sewer and water supply, electrical and telecommunications systems, plumbing, industrial as well as radiant heating systems.
This design manual covers the technical aspects of designing pressure pipe systems with PVC pipe. More specifically, municipal potable water systems, as well as irrigation and sewer force main systems are described.

The manual is organized into three sections:
Section 1 deals with specific products and includes detailed information on applications, dimensions and applicable standards for each system.

Section 2 deals with general design issues associated with PVC systems such as hydraulics, cyclic design and other topics that are applicable to all the products described in the manual.
Section 3 consists of design examples that apply the concepts from the first two sections.
This manual is designed for Engineers, Technologists and other municipal infrastructure professionals who require a deeper understanding of municipal piping systems than can be gleaned from the more general overview literature available from IPEX.



## Section One: Product Information

## Introduction

IPEX offers a number of different pressure piping systems that are used for various applications. While they are all plastic systems, they vary in outside diameter configurations and in available pressure ratings.

The products offered are:
Blue Brute ${ }^{\oplus}$ and IPEX Centurion ${ }^{\circledR}$ Piping Systems - Cast iron outside diameter (CIOD) pipe and fittings
CycleTough ${ }^{\circledR}$ Piping Systems - Iron Pipe Size outside diameter (IPSOD) pipe and fittings
TerraBrute ${ }^{\oplus}$ Pipe - CIOD pipe modified for use with trenchless installation methods such as directional drilling or pipe bursting Q-Line ${ }^{\oplus}$ Water Service Tubing -3/4" and 1" composite pipe designed for use as a water service to connect houses to main lines.

## Summary of Pressure Pipe and Fittings Testing

All IPEX pressure pipes and fittings are manufactured to standards from various recognized organizations such as the AWWA, CSA, ASTM and others. As a result, all pressure pipe products undergo a variety of testing and quality procedures.

## Blue Brute, IPEX Centurion, and TerraBrute Piping Systems

These piping systems are manufactured under various AWWA standards, including AWWA C900 (Blue Brute and TerraBrute), and AWWA C905 (IPEX Centurion). Fittings are manufactured under the C900, C905 and C907 standards.

Each length of Blue Brute, IPEX Centurion and TerraBrute pipe is hydrostatically tested in order to verify the pressure capabilities of each pipe as dictated by AWWA C900 and C905. In addition, burst tests are carried out regularly to verify the integrity of the pipe and joint system. It should be remembered that the hydrostatic test is done using the pipe's own gasket, which means that both the pipe and the joining system are being checked. AWWA standards also require a number of other tests, including impact tests at room temperature.

TerraBrute pipe does not strictly comply with AWWA C900/905 standards because of the dimensional change imposed by the grooving procedure, however it is tested using the same procedures as conventional Blue Brute and IPEX Centurion. The hydrostatic proof test is carried out on each length of TerraBrute to the same pressures and durations as for standard Blue Brute or IPEX Centurion.

In addition to AWWA requirements, CSA certification requires very stringent testing and QA/QC procedures. For example, the CSA B137.3 standard dictates that a vacuum test be performed on samples of pipe joints to verify that they can withstand a vacuum pressure of -10.8 psi . (Further tests have been performed by IPEX that simulate full vacuum pressures combined with external groundwater pressure of over 100 psi with no leakage).

CSA certification also requires impact testing to carried out at $0^{\circ} \mathrm{C}\left(32^{\circ} \mathrm{F}\right)$, which is a much tougher test compared to the room temperature testing required by the AWWA. This is an example of how one standard can have significantly tougher testing requirements than another

In addition to the pressure and impact testing, the material itself is tested by using acetone immersion tests and heat reversion tests. Both tests are used to check that the proper degree of fusion has occurred during the extrusion process.

The dimensional characteristics of each pipe and fitting are checked constantly during the extrusion and molding processes, and samples are taken for detailed dimensional analysis during each extrusion or molding run.

## CycleTough (IPSOD) Pipe

Cycletough pipe undergoes testing identical to that of IPEX Centurion pipe with the exception of the hydrostatic proof test of each length of pipe. This does not mean that the pipe is of any lesser quality than Blue Brute or IPEX Centurion pipe - it only means that it is manufactured under a different standard (ASTM D2241) that does not require the hydrostatic proof test.

In addition to performance and dimensional checks, National Sanitation Foundation (NSF) requirements mean that all products are thoroughly tested to ensure they have no effect on potable water.

To summarize - There are many standards governing the manufacture and design of IPEX pressure pipes and fittings. IPEX also has internal testing standards that are often well in excess of published requirements to ensure acceptable performance on the jobsite.

## Blue Brute® Piping Systems

Blue Brute is one of the most well known names in municipal water supply, as it has built up an enviable reputation for performance and reliability over the years. Blue Brute pipe and fittings eliminate the threat of corrosion, while providing reliable Iong-term service. While Blue Brute pipe is compatible with iron fittings, IPEX recommends the use of Blue Brute fittings as they are made to match the pipe, and eliminate the "Achilles heel" of many systems - corroding iron fittings.

It is advisable to specify pipe and fittings from the same manufacturer in order to ensure a completely matched system. For example, many competing PVC injection molded fittings are manufactured with
PVC compound with a lower hydrostatic design basis that the pipe. Only by specifying Blue Brute fittings can you ensure that the fittings have the same 4000 psi long term strength as the pipe itself.


## Applications:

Municipal water distribution systems and fire lines.
Irrigation, sewage forcemains, industrial lines.


## Blue Brute ${ }^{\circledR}$ Piping Systems cont’o

## Gasket Options For Contaminated Soils

Blue Brute pipe and fittings have removable gaskets. This allows oil resistant (nitrile) gaskets to be easily substituted when installing piping systems in contaminated soils (please refer to Section 2 - Chemical Permeation and Resistance for more information on this topic)

## Standards:

Blue Brute Pipe:
AWWA C900, CSA B137.3, Factory Mutual, ULC and ULI
Approved, NSF-61, Certified to NQ 36240-250


Blue Brute Fittings:
AWWA C907, CSA B137.2 (100mm - 200mm), AWWA C900, CSA B137.3 ( 250 mm -300mm), Factory Mutual, ULC and ULI Approved


## Short Form Specifications

## General

Blue Brute pipe shall conform to AWWA C900 "Poly (Vinyl Chloride) (PVC) Pressure Pipe (4" - 12") for Water," and certified to CSA B137.3 "Rigid Poly (Vinyl Chloride) (PVC) Pipe for Pressure Applications." Blue Brute DR25 shall have a pressure class of $690 \mathrm{kPa}(100 \mathrm{psi})$. DR18 pipe shall have a pressure class of $1,034 \mathrm{kPa}(150 \mathrm{psi})$. DR 14 pipe shall have a pressure class of $1,379 \mathrm{kPa}(200 \mathrm{psi})$.

## Material

Blue Brute pipe shall be made from clean, 12454B PVC compound, conforming to ASTM resin specification D1784.

## Product

Pipe shall be suitable for use at maximum hydrostatic working pressures equal to the class designation at $23^{\circ} \mathrm{C}$ $\left(73^{\circ} \mathrm{F}\right.$ ). Laying lengths shall be 6.1 meters ( 20 feet). Pipe shall have cast-iron outside diameters. Every length must be proof tested at four times the pressure.

## Joining

The gasket shall be carefully fitted to the bell groove if not already factory installed. Both bell and spigot shall be clean and free of debris before approved lubricant is applied. The pipe and/or fittings shall be joined by push-fitting bell and spigot joint to the depth line marked on the spigot. When pipe has been cut in the field, the end shall be made square and beveled to a $15^{\circ}$ chamfer. All insertion lines should be re-drawn, according to the IPEX Pressure Pipe Installation Guide.

## Molded Fittings

Blue Brute fittings shall conform to AWWA C907 "Polyvinyl Chloride (PVC) Pressure Fittings for Water (4" through 8")" and be certified to CSA B137.2 "PVC Injected Molded Gasketed Fittings for Pressure Applications." They shall also be UL Listed and FM approved.

## Fabricated Fittings

Fabricated fittings shall be made from segments of AWWA C900 Class 150 PVC pipe bonded together and over-wrapped with fiberglass-reinforced polyester. The pressure class must match the pipe. The fittings must meet the requirements of CSA B137.3.

## Lubricant

Pipe must be assembled with IPEX non-toxic, water soluble lubricant listed by the National Sanitation Foundation.

## Colour Coding

Water pipe and fittings shall be colour coded blue.

## Blue Brute ${ }^{\oplus}$ Piping Systems cont'o

## Dimensions:

Blue Brute pipes and fittings are manufactured with cast iron outside diameters (CIOD), which means that they are compatible with much of the existing infrastructure of older iron pipes. This means that no special transition fittings are needed with Blue Brute.

|  |  | *Class 100 (DR25) |  |  |  |  |  | Class 150 (DR18) |  |  |  |  |  | Class 200 (DR14) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Size |  | Avg. ID |  | Min. Wall Thickness |  | Avg. OD |  | Avg. ID |  | Min. Wall Thickness |  | Avg. OD |  | Avg. ID |  | Min. Wall Thickness |  | Avg. OD |  |
| in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm |
| 4 | 100 | 4.42 | 112 | 0.192 | 5 | 4.80 | 122 | 4.27 | 108 | 0.267 | 7 | 4.80 | 122 | 4.11 | 104 | 0.343 | 9 | 4.80 | 122 |
| 6 | 150 | 6.35 | 161 | 0.276 | 7 | 6.90 | 175 | 6.13 | 155 | 0.383 | 10 | 6.90 | 175 | 5.91 | 149 | 0.493 | 13 | 6.90 | 175 |
| 8 | 200 | 8.33 | 212 | 0.362 | 9 | 9.05 | 230 | 8.05 | 204 | 0.502 | 13 | 9.05 | 230 | 7.76 | 198 | 0.646 | 16 | 9.05 | 230 |
| 10 | 250 | 10.21 | 260 | 0.444 | 11 | 11.10 | 282 | 9.87 | 250 | 0.616 | 16 | 11.10 | 282 | 9.51 | 242 | 0.793 | 20 | 11.10 | 282 |
| 12 | 300 | 12.15 | 309 | 0.527 | 13 | 13.20 | 335 | 11.73 | 297 | 0.733 | 19 | 13.20 | 335 | 11.31 | 287 | 0.943 | 24 | 13.20 | 335 |

[^0]
## $90^{\circ}$ Elbow



| SIZE |  | A |  | B |  | C |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm |
| 4 | 100 | 10.14 | 257 | 6.25 | 159 | 10.14 | 257 |
| 6 | 150 | 13.90 | 353 | 8.88 | 226 | 13.90 | 353 |
| 8 | 200 | 16.90 | 430 | 11.36 | 289 | 16.90 | 430 |


$45^{\circ}$ Elbow

| SIZE |  | A |  | B |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm |
| 4 | 100 | 5.63 | 143 | 6.27 | 159 |
| 6 | 150 | 7.56 | 192 | 8.80 | 225 |
| 8 | 200 | 8.80 | 224 | 11.30 | 287 |

## Blue Brute ${ }^{\oplus}$ Piping Systems cont'o


22 $12^{\circ}$ Elbow

| SIZE |  | A |  | B |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm |
| 6 | 150 | 6.82 | 173 | 8.84 | 225 |
| 8 | 200 | 7.90 | 200 | 11.30 | 287 |

$111_{4}{ }^{\circ}$ Elbow

| SIZE |  | A |  | B |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm |
| 6 | 150 | 6.45 | 164 | 8.84 | 225 |
| 8 | 200 | 7.48 | 190 | 11.30 | 287 |

Reducing Adapter Spigot x Bell


| SIZE |  | A |  | B |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm |
| $6 \times 4$ | $150 \times 100$ | 5.8 | 147 | 4.3 | 109 |
| $8 \times 6$ | $200 \times 150$ | 12.5 | 318 | 5.5 | 140 |
| $10 \times 8$ | $250 \times 200$ | 7.3 | 185 | 5.8 | 147 |
| $12 \times 10$ | $300 \times 250$ | 10.1 | 256 | 6.5 | 165 |

Coupling (available without centerstop as a Repair Coupling)

| SIZE |  | A |  | B |  | C |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm |
| 4 | 100 | 8.18 | 207 | 6.27 | 160 | 0.25 | 7 |
| 6 | 150 | 12.11 | 307 | 8.88 | 225 | 0.25 | 7 |
| 8 | 200 | 13.58 | 345 | 11.35 | 288 | 0.25 | 7 |
| 10 | 250 | 18.12 | 460 | 14.30 | 363 | 0.50 | 13 |
| 12 | 300 | 19.40 | 493 | 17.30 | 439 | 0.50 | 13 |

## Blue Brute ${ }^{\oplus}$ Pifing Systems cont'o

## Single Tapped Coupling



| SIZE |  | A |  | B |  | C |  | D |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | in | mm |
| $4 \times 4 \times$ | $100 \times 100 \times$ | $3 / 4$ | 20 | 6.27 | 159 | 10.20 | 259 | 4.43 | 113 |
| $4 \times 4 \times$ | $100 \times 100 \times$ | 1 | 25 | 6.27 | 159 | 10.20 | 259 | 4.43 | 113 |
| $6 \times 6 \times$ | $150 \times 150 \times$ | $3 / 4$ | 20 | 8.74 | 222 | 14.38 | 365 | 6.06 | 154 |
| $6 \times 6 \times$ | $150 \times 150 \times$ | 1 | 25 | 8.74 | 222 | 14.38 | 365 | 6.06 | 154 |
| $6 \times 6 \times$ | $150 \times 150 \times$ | $1-1 / 2$ | 40 | 8.74 | 222 | 14.38 | 365 | 6.06 | 154 |
| $6 \times 6 \times$ | $150 \times 150 \times$ | 2 | 50 | 8.74 | 222 | 14.38 | 365 | 6.06 | 154 |
| $8 \times 8 \times$ | $200 \times 200 \times$ | $3 / 4$ | 20 | 11.30 | 287 | 15.00 | 381 | 7.91 | 201 |
| $8 \times 8 \times$ | $200 \times 200 \times$ | 1 | 25 | 11.30 | 287 | 15.00 | 381 | 7.91 | 201 |
| $8 \times 8 \times$ | $200 \times 200 \times$ | $1-1 / 2$ | 40 | 11.30 | 287 | 15.00 | 381 | 7.91 | 201 |
| $8 \times 8 \times$ | $200 \times 200 \times$ | 2 | 50 | 11.30 | 287 | 15.00 | 381 | 7.91 | 201 |



| SIZE |  | A |  |
| :---: | :---: | :---: | :---: |
| in | mm | in | mm |
| 4 | 100 | 5.9 | 150 |
| 6 | 150 | 7.0 | 178 |
| 8 | 200 | 8.1 | 206 |
| 10 | 250 | 9.0 | 228 |
| 12 | 300 | 9.8 | 249 |

## Blue Brute ${ }^{\oplus}$ Piping Systems cont'o

Double Tapped Coupling


Note: 3/4 inch (20 mm) Taps to 2 inch ( 50 mm )

Taps: AWWA Thread

| SIZE |  | A |  | B |  | C |  | D |  | E |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | in | mm | in | mm |
| $6 x^{3} / 4 x^{3} / 4$ | $150 \times 20 \times 20$ | 14.38 | 365 | 8.74 | 222 | $3 / 4$ | 20 | 6.06 | 154 | 0.75 | 20 |
| $6 \times 1 x^{3}$ | $150 \times 25 \times 20$ | 14.38 | 365 | 8.74 | 22 | 1 | 25 | 6.06 | 154 | 0.75 | 20 |
| $6 \times 1 \times 1$ | $150 \times 25 \times 25$ | 14.38 | 365 | 8.74 | 222 | 1 | 25 | 6.06 | 154 | 1 | 25 |
| $6 \times 1^{1 / 4} \mathrm{X}^{3 / 4}$ | $150 \times 32 \times 20$ | 14.38 | 365 | 8.74 | 222 | $11 / 4$ | 32 | 6.06 | 154 | 0.75 | 20 |
| $6 \times 1^{1 / 4 \times 1}$ | $150 \times 32 \times 25$ | 14.38 | 365 | 8.74 | 222 | $11 / 4$ | 32 | 6.06 | 154 | 1 | 25 |
| $6 \times 1^{1 / 2} \mathrm{X}^{3 / 4}$ | $150 \times 40 \times 20$ | 14.38 | 365 | 8.74 | 222 | 1 | 40 | 6.06 | 154 | 0.75 | 20 |
| $6 \times 1^{1 / 2} \times 1$ | $150 \times 40 \times 25$ | 14.38 | 365 | 8.74 | 222 | $1^{1 / 2}$ | 40 | 6.06 | 154 | 1 | 25 |
| $6 \times 2 x^{3} / 4$ | $150 \times 50 \times 20$ | 14.38 | 365 | 8.74 | 222 | 2 | 50 | 6.06 | 154 | 0.75 | 20 |
| $6 \times 2 \times 1$ | $150 \times 50 \times 25$ | 14.38 | 365 | 8.74 | 222 | 2 | 50 | 6.06 | 154 | 1 | 25 |
| $8 x^{3} / 4 x^{3} / 4$ | $200 \times 20 \times 20$ | 15.00 | 381 | 11.30 | 287 | $3 / 4$ | 20 | 7.91 | 201 | 0.75 | 20 |
| $8 \times 1 x^{3} / 4$ | $200 \times 25 \times 20$ | 15.00 | 381 | 11.30 | 287 | 1 | 25 | 7.91 | 201 | 0.75 | 20 |
| $8 \times 1 \times 1$ | $200 \times 25 \times 25$ | 15.00 | 381 | 11.30 | 287 | 1 | 25 | 7.91 | 201 | 1 | 25 |
| $8 \times 1^{1 / 4} \mathrm{X}^{3 / 4}$ | $200 \times 32 \times 20$ | 15.00 | 381 | 11.30 | 287 | $11 / 4$ | 32 | 7.91 | 201 | 0.75 | 20 |
| $8 \times 1^{1 / 4 \times 1}$ | $200 \times 32 \times 25$ | 15.00 | 381 | 11.30 | 287 | $1^{1 / 4}$ | 32 | 7.91 | 201 | 1 | 25 |
| $8 \times 1^{1 / 2} x^{3 / 4}$ | $200 \times 40 \times 20$ | 15.00 | 381 | 11.30 | 287 | $11 / 2$ | 40 | 7.91 | 201 | 0.75 | 20 |
| $8 \times 1^{1 / 2} \times 1$ | $200 \times 40 \times 25$ | 15.00 | 381 | 11.30 | 287 | $1^{1 / 2}$ | 40 | 7.91 | 201 | 1 | 25 |
| $8 \times 2 x^{3} / 4$ | $200 \times 50 \times 20$ | 15.00 | 381 | 11.30 | 287 | 2 | 50 | 7.91 | 201 | 0.75 | 20 |
| $8 \times 2 \times 1$ | $200 \times 50 \times 25$ | 15.00 | 381 | 11.30 | 287 | 2 | 50 | 7.91 | 201 | 1 | 25 |

Tee


| SIZE |  | A |  | B |  | C |  | D |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm | in | mm |
| $4 \times 4 \times 4$ | $100 \times 100 \times 100$ | 14.04 | 357 | 6.27 | 159 | 10.15 | 258 | 4.88 | 124 |
| $6 \times 6 \times 4$ | $150 \times 150 \times 100$ | 16.99 | 432 | $8.88 \times 6.27$ | $226 \times 159$ | 12.43 | 316 | 6.93 | 176 |
| $6 \times 6 \times 6$ | $150 \times 150 \times 150$ | 18.92 | 481 | 8.88 | 226 | 13.90 | 353 | 6.93 | 176 |
| $8 \times 8 \times 4$ | $200 \times 200 \times 100$ | 18.55 | 471 | $11.37 \times 6.27$ | $289 \times 159$ | 14.68 | 373 | 9.13 | 232 |
| $8 \times 8 \times 6$ | $200 \times 200 \times 150$ | 20.48 | 520 | $11.37 \times 8.88$ | $289 \times 226$ | 16.14 | 410 | 9.13 | 232 |
| $8 \times 8 \times 8$ | $200 \times 200 \times 200$ | 22.46 | 571 | 11.37 | 289 | 16.91 | 430 | 9.13 | 232 |

## IPEX Centurion ${ }^{\circledR}$ Piping Systems

IPEX Centurion extends the corrosion-free benefits of Blue Brute to larger diameters of pipe and new applications. The versatility and ease of installation of IPEX Centurion is unmatched - shop drawings are eliminated and costly and difficult to install corrosion protection can be eliminated. In addition, unlike HDPE or concrete pressure pipe, every length of IPEX Centurion is tested to double its pressure rating.


## Applications:

Water transmission lines, forcemains.
Irrigation, gravity lines, industrial lines


## IPEX Centurion ${ }^{\oplus}$ Piping Systems cont’o

## Pressure Ratings

IPEX Centurion can withstand extremely high short term pressures, in addition to lower levels of long-term pressure. As a result, the AWWA M23 Manual includes both long term pressure ratings (LTR) and short term ratings (STR).

| SDR | Short Term Rating <br> STR* (2.5:1 S.F.) (psi) | Long Term Rating <br> LTR* (2:1 S.F.) (psi) |
| :---: | :---: | :---: |
| 51 | 100 | 80 |
| 41 | 130 | 100 |
| 32.5 | 165 | 125 |
| 26 | 205 | 160 |
| 25 | 215 | 165 |
| 18 | 300 | 235 |
| 14 | 395 | 305 |

Note: Values have been rounded to the nearest 5 psi

## Surge Pressures in IPEX Centurion

Transient pressures in pipelines occur as a result of the fluid velocity changing over a relatively short time. The method for approximating a surge pressure is described in section 2, however it should be noted that for most large diameter pipelines, a formal transient analysis should be carried out by a qualified person in order to fully understand the effects of transients in any given system. The method shown in section 2 is certainly appropriate for initial design purposes however.

The table below shows the surge pressure generated assuming an instantaneous stoppage of a flow moving at 0.3 $\mathrm{m} / \mathrm{s}(1 \mathrm{ft} / \mathrm{s})$.

| SDR | Surge Pressure (psi) |
| :---: | :---: |
| 51 | 10.8 |
| 41 | 11.4 |
| 32.5 | 12.8 |
| 26 | 14.5 |
| 25 | 14.7 |
| 14 | 17.4 |



## IPEX Centurion ${ }^{\oplus}$ Piping Systems cont'o

## IPEX Centurion for Gravity Applications

With its pressure rated joints and non-corroding construction, IPEX Centurion- is a natural choice for gravity flow lines. When designing any flexible conduit application, the ring deflection should be calculated for the applicable loading conditions. The table below shows the ring deflections for a variety of different SDR configurations based on depth of bury and H2O loading. For more information on how to calculate ring deflections on PVC pipe, please refer to the IPEX Sewer Design Manual.

1. Deflection values shown include effect of H 2 O live load and dead load.
2. External loading based upon a prism load of soil weight of 120 lbs. per cubic foot ( $1900 \mathrm{~kg} / \mathrm{m} 3$ ).
3. Bedding classifications correspond to ASTM D2321.
4. The deflection lag factor is 1.0 for a prism load.
5. DR18 deflections have not been shown because they are insignificant in most cases.
6. Recommended maximum deflection is $7.5 \%$.

Contact IPEX for applications where greater deflections are anticipated.
7. $\mathrm{n} / \mathrm{r}$ - not recommended for H 2 O live load (ok with dead load)

## Standards:

AWWA C905, CSA B137.3, NQ 3624-250, NSF-61
Factory Mutual:
SDR18 is FM approved to 500 mm diameter (20")
Underwriter's Laboratories 1218:
SDR18 is listed to 600 mm diameter (24")
SDR25 is listed to 750 mm diameter (30")


## Short Form Specifications

## General

Pipe must conform to AWWA C905 and be certified to CSA B137.3 "Rigid Poly (Vinyl Chloride) (PVC) Pipe for Pressure Applications." DR51, 41, 32.5, 25, 18, and 14 pipe must have the following pressure ratings: $80 \mathrm{psi}(550 \mathrm{kPa}), 100$ psi ( 690 kPa ), $125 \mathrm{psi}(860 \mathrm{kPa}), 165 \mathrm{psi}(1140 \mathrm{kPa})$, 235 psi ( 1620 kPa ) and $305 \mathrm{psi}(2100 \mathrm{kPa})$. For pressure applications, each length of pipe must be hydro-tested at twice the rating and a short-term pressure test must be conducted once per production run. Pipe to be IPEX Centurion or approved equal.

## Fabricated Fittings

Fabricated fittings shall be made from segments of AWWA C905 pipe that are butt fused or bonded together and overwrapped with fiberglass-reinforced polyester. the fittings must always meet the pressure rating of the pipe system.

## Table 1 - Percent (\%) Deflection for IPEX Centurion Pressure Pipe

| ASTM EMBEDMENT MATERIAL CLASSIFICATION |  | DENSITY (PROCTOR) AASHO T-99 | $\begin{gathered} \mathrm{E}^{\prime} \\ \mathrm{psi} \\ (\mathrm{kPa}) \end{gathered}$ | DR | HEIGHT OF COVER |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \hline(\mathrm{ft} .) 1 \\ & (\mathrm{~m}) 0.3 \end{aligned}$ |  |  | $\begin{gathered} 2 \\ 0.6 \end{gathered}$ | $\begin{gathered} 4 \\ 1.2 \end{gathered}$ | $\begin{gathered} 6 \\ 1.8 \end{gathered}$ | $\begin{gathered} 8 \\ 2.4 \end{gathered}$ | $\begin{aligned} & 10 \\ & 30 \end{aligned}$ | $\begin{aligned} & 15 \\ & 4.6 \end{aligned}$ | $\begin{aligned} & 20 \\ & 6.1 \end{aligned}$ | $\begin{aligned} & 25 \\ & 7.6 \end{aligned}$ | $\begin{aligned} & 30 \\ & 9.1 \end{aligned}$ | $\begin{gathered} 35 \\ 10.7 \end{gathered}$ | $\begin{gathered} 40 \\ 12.2 \end{gathered}$ | $\begin{gathered} 45 \\ 13.7 \end{gathered}$ | $\begin{gathered} 50 \\ 15.2 \end{gathered}$ |
| Manufactured | CLASS I |  | 90\% | $\begin{gathered} 3,000 \\ (20700) \end{gathered}$ | 51 | $\mathrm{n} / \mathrm{r}$ | 0.5 | 0.3 | 0.4 | 0.4 | 0.5 | 0.7 | 0.9 | 1.1 | 1.4 | 1.6 | 1.8 | 2.0 | 2.3 |
| Granular |  | 41 |  |  | $\mathrm{n} / \mathrm{r}$ | 0.5 | 0.3 | 0.4 | 0.4 | 0.4 | 0.7 | 0.9 | 1.1 | 1.3 | 1.6 | 1.8 | 2.0 | 2.2 |
| Angular |  | 32.5 |  |  | 0.7 | 0.5 | 0.3 | 0.3 | 0.4 | 0.4 | 0.7 | 0.9 | 1.1 | 1.3 | 1.5 | 1.7 | 2.0 | 2.2 |
|  |  | 25 |  |  | 0.7 | 0.5 | 0.3 | 0.3 | 0.4 | 0.4 | 0.6 | 0.8 | 1.0 | 1.2 | 1.4 | 1.6 | 1.9 | 2.1 |
| Clean Sand \& Gravel | CLASS II | 90\% | $\begin{gathered} 2,000 \\ (13000) \end{gathered}$ | 51 | $\mathrm{n} / \mathrm{r}$ | 0.7 | 0.5 | 0.5 | 0.6 | 0.7 | 1.0 | 1.3 | 1.7 | 2.0 | 2.3 | 2.7 | 3.0 | 3.4 |
|  |  |  |  | 41 | $\mathrm{n} / \mathrm{r}$ | 0.7 | 0.5 | 0.5 | 0.6 | 0.7 | 1.0 | 1.3 | 1.7 | 2.0 | 2.3 | 2.6 | 3.0 | 3.3 |
|  |  |  |  | 32.5 | 1.0 | 0.7 | 0.5 | 0.5 | 0.5 | 0.6 | 1.0 | 1.3 | 1.6 | 1.9 | 2.2 | 2.6 | 2.9 | 3.2 |
|  |  |  |  | 25 | 1.0 | 0.7 | 0.4 | 0.5 | 0.5 | 0.6 | 0.9 | 1.2 | 1.5 | 1.8 | 2.1 | 2.4 | 2.7 | 2.9 |
|  |  | 80\% | $\begin{gathered} 1,000 \\ (7000) \end{gathered}$ | 51 | $\mathrm{n} / \mathrm{r}$ | 1.5 | 1.0 | 1.1 | 1.1 | 1.3 | 2.0 | 2.6 | 3.3 | 4.0 | 4.6 | 5.3 | 5.9 | 6.6 |
|  |  |  |  | 41 | $\mathrm{n} / \mathrm{r}$ | 1.4 | 1.0 | 1.0 | 1.1 | 1.3 | 1.9 | 2.6 | 3.2 | 3.8 | 4.5 | 5.1 | 5.8 | 6.4 |
|  |  |  |  | 32.5 | 2.0 | 1.3 | 0.9 | 1.0 | 1.0 | 1.2 | 1.8 | 2.4 | 3.0 | 3.6 | 4.2 | 4.8 | 5.4 | 6.0 |
|  |  |  |  | 25 | 1.7 | 1.1 | 0.8 | 0.8 | 0.9 | 1.0 | 1.6 | 2.1 | 2.6 | 3.1 | 3.6 | 4.2 | 4.7 | 5.2 |
| Sand \& Grave with Fines | CLASS III | 90\% | $\begin{gathered} 1,000 \\ (7000) \end{gathered}$ | 51 | $\mathrm{n} / \mathrm{r}$ | 1.5 | 1.0 | 1.1 | 1.1 | 1.3 | 2.0 | 2.6 | 3.3 | 4.0 | 4.6 | 5.3 | 5.9 | 6.6 |
|  |  |  |  | 41 | $\mathrm{n} / \mathrm{r}$ | 1.4 | 1.0 | 1.0 | 1.1 | 1.3 | 1.9 | 2.6 | 3.2 | 3.8 | 4.5 | 5.1 | 5.8 | 6.4 |
|  |  |  |  | 32.5 | 2.0 | 1.3 | 0.9 | 1.0 | 1.0 | 1.2 | 1.8 | 2.4 | 3.0 | 3.6 | 4.2 | 4.8 | 5.4 | 6.0 |
|  |  |  |  | 25 | 1.7 | 1.1 | 0.8 | 0.8 | 0.9 | 1.0 | 1.6 | 2.1 | 2.6 | 3.1 | 3.6 | 4.2 | 4.7 | 5.2 |
|  |  | 85\% | $\begin{gathered} 500 \\ (3500) \end{gathered}$ | 51 | n/r | $\mathrm{n} / \mathrm{r}$ | 1.9 | 2.0 | 2.2 | 2.6 | 3.8 | 5.1 | 6.4 | 7.7 | 8.9 | 10.2 | 11.5 | 12.8 |
|  |  |  |  | 41 | $\mathrm{n} / \mathrm{r}$ | $\mathrm{n} / \mathrm{r}$ | 1.8 | 1.9 | 2.1 | 2.4 | 3.6 | 4.8 | 6.0 | 7.2 | 8.4 | 9.6 | 10.8 | 12.0 |
|  |  |  |  | 32.5 | $\mathrm{n} / \mathrm{r}$ | 2.4 | 1.6 | 1.7 | 1.8 | 2.1 | 3.2 | 4.3 | 5.3 | 6.4 | 7.5 | 8.5 | 9.6 | 10.7 |
|  |  |  |  | 25 | $\mathrm{n} / \mathrm{r}$ | 1.9 | 1.3 | 1.3 | 1.4 | 1.7 | 2.5 | 3.3 | 4.2 | 5.0 | 5.9 | 6.7 | 7.5 | 8.4 |
| Silt \& Clay | CLASS IV | 85\% | $\begin{gathered} 400 \\ (2760) \end{gathered}$ | 51 | $\mathrm{n} / \mathrm{r}$ | $\mathrm{n} / \mathrm{r}$ | 2.4 | 2.5 | 2.7 | 3.1 | 4.7 | 6.3 | 7.9 | 9.4 | 11.0 | 12.6 | 14.1 | 15.7 |
|  |  |  |  | 41 | $\mathrm{n} / \mathrm{r}$ | n/r | 2.2 | 2.3 | 2.5 | 2.9 | 4.4 | 5.8 | 7.3 | 8.8 | 10.2 | 11.7 | 13.1 | 14.6 |
|  |  |  |  | 32.5 | $n / r$ | 2.8 | 1.9 | 2.0 | 2.2 | 2.5 | 3.8 | 5.1 | 6.3 | 7.6 | 8.9 | 10.1 | 11.4 | 12.7 |
|  |  |  |  | 25 | $\mathrm{n} / \mathrm{r}$ | 2.1 | 1.4 | 1.5 | 1.6 | 1.9 | 2.9 | 3.8 | 4.8 | 5.7 | 6.7 | 7.6 | 8.6 | 9.5 |

## IPEX Centurion® Piping Systems cont'o

## Dimensions

IPEX Centurion is manufactured with a cast iron outside diameter (CIOD) so it is compatible with much of the existing older infrastructure of iron pipes. In addition, IPEX Centurion can be field cut, which means unexpected changes in the field can be accommodated quickly, without having to wait for new shop drawings.

IPEX Centurion Fittings are manufactured using sections of AWWA C905 pipe, overwrapped with a layer of fibre reinforced plastic (FRP). While IPEX Centurion is compatible with iron fittings, IPEX recommends the use of IPEX Centurion fittings exclusively with IPEX Centurion pipe.

|  |  | *PR 80 (DR51) |  |  |  |  |  | *PR100 (DR41) |  |  |  |  |  | *PR 125 (DR32.5) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Size |  | Avg. ID |  | Min. Wall Thickness |  | Avg. OD |  | Avg. ID |  | Min. Wall Thickness |  | Avg. OD |  | Avg. ID |  | Min. Wall Thickness |  | Avg. OD |  |
| in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm |
| 14 | 350 | - | - | - | - | - | - | 14.6 | 369.7 | 0.37 | 9.5 | 15.3 | 388.6 | - | - | - | - | - | - |
| 16 | 400 | - | - | - | - | - | - | 16.6 | 420.4 | 0.43 | 10.8 | 17.4 | 442.0 | - | - | - | - | - | - |
| 18 | 450 | 18.7 | 475.9 | 0.38 | 9.7 | 19.5 | 495.3 | 18.5 | 471.1 | 0.48 | 12.1 | 19.5 | 495.3 | - | - | - | - | - | - |
| 20 | 500 | 20.8 | 527.0 | 0.42 | 10.8 | 21.6 | 548.6 | 20.5 | 521.8 | 0.53 | 13.4 | 21.6 | 548.6 | - | - | - | - | - | - |
| 24 | 600 | 24.8 | 629.6 | 0.50 | 12.8 | 25.8 | 655.3 | 24.5 | 623.3 | 0.63 | 16.0 | 25.8 | 655.3 | 24.2 | 615.0 | 0.80 | 20.2 | 25.8 | 655.3 |
| 30 | 750 | 30.7 | 780.9 | 0.63 | 15.9 | 32.0 | 812.8 | 30.4 | 773.2 | 0.78 | 19.8 | 32.0 | 812.8 | 30.0 | 762.8 | 0.98 | 25.0 | 32.0 | 812.8 |
| 36 | 900 | 36.8 | 934.7 | 0.75 | 19.1 | 38.3 | 972.8 | 36.4 | 925.3 | 0.93 | 23.7 | 38.3 | 972.8 | 35.9 | 912.9 | 1.18 | 29.9 | 38.3 | 972.8 |
| 42 | 1050 | 42.6 | 1082.8 | 0.87 | 22.2 | 44.5 | 1130.3 | 42.2 | 1071.4 | 1.09 | 27.5 | 44.5 | 1130.3 | 41.6 | 1056.6 | 1.37 | 34.8 | 44.5 | 1130.3 |
| 48 | 1200 | 48.7 | 1236.2 | 1.00 | 25.3 | 50.8 | 1290.3 | 48.2 | 1223.0 | 1.24 | 31.5 | 50.8 | 1290.3 | - | - | - | - | - | - |

* Pressure rating includes a 2:1 safety factor.

|  |  | PR 165 (DR25) |  |  |  |  |  | PR 235 (DR18) |  |  |  |  |  | PR 305 (DR14) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Size |  | Avg. ID |  | Min. Wall Thickness |  | Avg. OD |  | Avg. ID |  | Min. Wall <br> Thickness |  | Avg. OD |  | Avg. ID |  | Min. Wall Thickness |  | Avg. OD |  |
| in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm |
| 14 | 350 | 14.1 | 357.5 | 0.61 | 15.5 | 15.3 | 388.6 | 13.6 | 345.4 | 0.85 | 21.6 | 15.3 | 388.6 | 13.1 | 333.0 | 1.09 | 27.8 | 15.3 | 388.6 |
| 16 | 400 | 16.0 | 406.6 | 0.70 | 17.7 | 17.4 | 442.0 | 15.5 | 392.9 | 0.97 | 24.6 | 17.4 | 442.0 | 14.9 | 378.8 | 1.24 | 31.6 | 17.4 | 442.0 |
| 18 | 450 | 17.9 | 455.7 | 0.78 | 19.8 | 19.5 | 495.3 | 17.3 | 440.3 | 1.08 | 27.5 | 19.5 | 495.3 | - | - | - | - | - | - |
| 20 | 500 | 19.9 | 504.7 | 0.86 | 21.9 | 21.6 | 548.6 | 19.2 | 487.6 | 1.20 | 30.5 | 21.6 | 548.6 | - | - | - | - | - | - |
| 24 | 600 | 23.7 | 602.9 | 1.03 | 26.2 | 25.8 | 655.3 | 22.9 | 582.5 | 1.43 | 36.4 | 25.8 | 655.3 | - | - | - | - | - | - |
| 30 | 750 | 29.4 | 747.8 | 1.28 | 32.5 | 32.0 | 812.8 | - | - | - | - | - | - | - | - | - | - | - | - |
| 36 | 900 | 35.2 | 895.0 | 1.53 | 38.9 | 38.3 | 972.8 | - | - | - | - | - | - | - | - | - | - | - | - |
| 42 | 1050 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 48 | 1200 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |  |

## CycleTough ${ }^{\oplus}$ Piping Systems

CycleTough piping systems are specially designed for applications where pressures are expected to cycle up and down repeatedly, such as sewage forcemains, irrigation systems and other applications. One of the most important things to remember with CycleTough systems is that the fittings are made with PVC compound that has the same hydrostatic design basis (HDB) as the pipe. Most competing PVC fittings are made with compound having a significantly lower HDB, thus potentially compromising the system performance. Always specify a complete system of pipes and fittings from the same manufacturer to ensure matching fittings.


## Applications:

Forcemains, irrigation.
Rural water supply, water distribution and transmission.

## CycleTough ${ }^{\oplus}$ Piping Systems cont'o

## Pressure Ratings

CycleTough pipe is available in long term various pressure ratings, from 100 to 200 psi:

| SDR | Short Term Rating <br> (STR) | Long Term Rating <br> (LTR) |
| :---: | :---: | :---: |
| 41 | 130 | 100 |
| 32.5 | 165 | 125 |
| 26 | 205 | 160 |
| 21 | 255 | 200 |

For more information on how these ratings are calculated, please refer to section 3.

## Standards

## CycleTough Pipe

Certified to CSA B137.3 - Rigid Poly (Vinyl Chloride) (PVC) Pipe for Pressure Applications
ASTM D2241 - Poly (Vinyl Chloride) (PVC) Plastic Pipe (SDR-PR) PVC

NSF-PW - NSF approved for potable water
Conforms to AWWA C905 - except for the hydrostatic test of each pipe length


## CycleTough Fittings

Certified to CSA B137.3
Various ASTM Standards
NSF-61


CNSF

## Short Form Specifications

IPSOD PVC Pipe shall be manufactured from PVC compound with an ASTM Cell class of 12454B. PVC Compound will have a minimum long term hydrostatic design basis of 4000 psi and a short term HDB of 6400 psi. Pipe shall be certified to CSA B137.3.

Injection molded PVC fittings shall be made from PVC compound with a minimum long term HDB of 4000 psi.

Fabricated fittings shall be made from sections of pipe certified to CSA B137.3, and shall also be certified to CSA B137.3.

All pipes and fittings shall be NSF-61 approved and color coded white.


## CycleTough ${ }^{\oplus}$ Piping Systems cont'o

## Dimensions

CycleTough pipe and fittings are manufactured with an Iron Pipe Size outside diameter (IPSOD). This outside diameter
configuration is consistent with that used for Schedule piping (sch. 40 and 80 ) as well as steel pipe sizes.

|  |  | Series 100 (SDR41) |  |  |  |  |  | Series 125 (SDR32.5) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Size |  | Avg. ID |  | Min. Wall Thickness |  | Avg. OD |  | Avg. ID |  | Min. Wall Thickness |  | Avg. OD |  |
| in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm |
| 3 | 75 | - | - | - | - | - | - | 3.271 | 83.09 | . 108 | 2.74 | 3.50 | 88.9 |
| 4 | 100 | 4.278 | 108.41 | . 109 | 2.78 | 4.50 | 114.3 | 4.208 | 106.88 | . 138 | 3.50 | 4.50 | 114.3 |
| 6 | 150 | 6.282 | 159.57 | . 162 | 4.12 | 6.63 | 168.3 | 6.194 | 157.32 | . 204 | 5.18 | 6.63 | 168.3 |
| 8 | 200 | 8.180 | 207.77 | . 209 | 5.32 | 8.62 | 219.1 | 8.063 | 204.80 | . 265 | 6.72 | 8.62 | 219.1 |
| 10 | 250 | 10.194 | 258.93 | . 262 | 6.66 | 10.75 | 273.1 | 10.049 | 255.24 | . 331 | 8.40 | 10.75 | 273.1 |
| 12 | 300 | 12.093 | 307.15 | . 311 | 7.90 | 12.75 | 323.9 | 11.921 | 302.78 | . 392 | 9.96 | 12.75 | 323.9 |
| 14 | 350 | 13.277 | 337.24 | . 341 | 8.66 | 14.00 | 355.6 | 13.090 | 332.49 | . 429 | 10.90 | 14.00 | 355.6 |
| 16 | 400 | 15.174 | 385.41 | . 390 | 9.90 | 16.00 | 406.4 | 14.957 | 379.90 | . 492 | 12.50 | 16.00 | 406.4 |
| 18 | 450 | 17.074 | 433.67 | . 437 | 11.10 | 18.00 | 457.2 | 16.823 | 427.31 | . 555 | 14.10 | 18.00 | 457.2 |
| 20 | 500 | 18.985 | 481.71 | . 488 | 12.40 | 20.00 | 508.0 | 18.698 | 474.93 | . 614 | 15.60 | 20.00 | 508.0 |
| 24 | 600 | 22.756 | 578.01 | . 587 | 14.90 | 24.00 | 609.6 | 22.431 | 569.74 | . 740 | 18.80 | 24.00 | 609.6 |


|  |  | Series 160 (SDR26) |  |  |  |  |  | Series 200 (SDR21) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Size |  | Avg. ID |  | Min. Wall Thickness |  | Avg. OD |  | Avg. ID |  | Min. Wall Thickness |  | Avg. OD |  |
| in | mm | in | mm | in | mm | in | mm | in | mm | in | mm | in | mm |
| 1-1/2 | 40 | 1.731 | 43.97 | . 080 | 2.02 | 1.90 | 48.3 | 1.709 | 43.42 | . 090 | 2.28 | 1.90 | 48.3 |
| 2 | 50 | 2.184 | 55.47 | . 091 | 2.30 | 2.38 | 60.4 | 2.137 | 54.29 | . 113 | 2.86 | 2.38 | 60.4 |
| 2-1/2 | 65 | 2.642 | 67.11 | . 109 | 2.78 | 2.87 | 73.0 | 2.584 | 65.62 | . 137 | 3.48 | 2.87 | 73.0 |
| 3 | 75 | 3.215 | 81.65 | . 135 | 3.42 | 3.50 | 88.9 | 3.146 | 79.91 | . 167 | 4.24 | 3.50 | 88.9 |
| 4 | 100 | 4.134 | 105.01 | . 172 | 4.38 | 4.50 | 114.3 | 4.046 | 102.77 | . 214 | 5.44 | 4.50 | 114.3 |
| 6 | 150 | 6.085 | 154.56 | . 255 | 6.48 | 6.63 | 168.3 | 5.957 | 151.30 | . 316 | 8.02 | 6.63 | 168.3 |
| 8 | 200 | 7.921 | 201.20 | . 331 | 8.42 | 8.62 | 219.1 | 7.756 | 197.00 | . 409 | 10.40 | 8.62 | 219.1 |
| 10 | 250 | 9.874 | 250.79 | . 413 | 10.50 | 10.75 | 273.1 | 9.665 | 245.49 | . 512 | 13.00 | 10.75 | 273.1 |
| 12 | 300 | 11.717 | 297.61 | . 488 | 12.40 | 12.75 | 323.9 | 11.467 | 291.25 | . 606 | 15.40 | 12.75 | 323.9 |
| 14 | 350 | 12.857 | 326.56 | . 539 | 13.70 | 14.00 | 355.6 | 12.589 | 319.77 | . 665 | 16.90 | 14.00 | 355.6 |
| 16 | 400 | 14.698 | 373.33 | . 614 | 15.60 | 16.00 | 406.4 | 14.381 | 365.27 | . 764 | 19.40 | 16.00 | 406.4 |
| 18 | 450 | 16.531 | 419.89 | . 693 | 17.60 | 18.00 | 457.2 | 16.180 | 410.98 | . 858 | 21.80 | 18.00 | 457.2 |
| 20 | 500 | 18.364 | 466.45 | . 772 | 19.60 | 20.00 | 508.0 | 17.980 | 456.70 | . 953 | 24.20 | 20.00 | 508.0 |
| 24 | 600 | 22.039 | 559.78 | . 925 | 23.50 | 24.00 | 609.6 | 21.580 | 548.12 | 1.142 | 29.00 | 24.00 | 609.6 |

## CycleTough ${ }^{\ominus}$ Piping Systems cont'o



| SIZE |  | L |  | $R$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm |
| 2 | 50 | 1.18 | 29.5 | 0.75 | 18.8 |
| $2-1 / 2$ | 65 | 1.80 | 45.0 | 1.00 | 25.0 |
| 3 | 75 | 2.00 | 50.0 | 1.00 | 25.0 |
| 4 | 100 | 2.20 | 55.0 | 1.00 | 25.0 |
| 6 | 150 | 2.80 | 70.0 | 1.25 | 31.3 |
| 8 | 200 | 4.87 | 121.8 | 1.50 | 37.5 |

$45^{\circ}$ Elbow G x G


| SIZE |  | L |  | $R$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm |
| 2 | 50 | 0.60 | 15.0 | 0.75 | 18.8 |
| $2-1 / 2$ | 65 | 1.80 | 45.0 | 1.00 | 25.0 |
| 3 | 75 | 1.12 | 28.0 | 1.00 | 25.0 |
| 4 | 100 | 1.10 | 27.5 | 1.00 | 25.0 |
| 6 | 150 | 1.60 | 40.0 | 1.25 | 31.3 |
| 8 | 200 | 2.40 | 60.0 | 1.50 | 37.5 |

Tee $\mathbf{G x} \mathbf{~ G ~ X ~ G ~}$


| SIZE |  | C |  | H |  | L |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm |
| 2 | 50 | 1.30 | 32.5 | 1.10 | 27.5 | 7.60 | 190.0 |
| $2-1 / 2$ | 65 | 1.67 | 41.8 | 1.63 | 40.8 | 9.50 | 237.5 |
| 3 | 75 | 1.99 | 49.8 | 1.99 | 49.8 | 10.80 | 270.0 |
| 4 | 100 | 2.57 | 64.3 | 2.65 | 66.3 | 12.50 | 312.5 |
| 6 | 150 | 3.76 | 94.0 | 3.77 | 94.3 | 14.90 | 372.5 |
| 8 | 200 | 4.91 | 122.8 | 4.91 | 122.8 | 21.65 | 541.3 |

## CycleTough ${ }^{\oplus}$ Piping Systems cont'o

Tap Service Tee - NPT Outlet

| SIZE |  | C |  | H |  | L |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm |
| $2 \times 1 / 2$ | $50 \times 15$ | 1.40 | 35.0 | 2.15 | 53.8 | 7.10 | 177.5 |
| $2 \times 3 / 4$ | $50 \times 20$ | 1.40 | 35.0 | 2.15 | 53.8 | 7.10 | 177.5 |
| $2 \times 1$ | $50 \times 25$ | 1.40 | 35.0 | 2.15 | 53.8 | 7.10 | 177.5 |
| $2 \times 1-1 / 4$ | $50 \times 32$ | 1.40 | 35.0 | 2.15 | 53.8 | 7.10 | 177.5 |
| $2 \times 1-1 / 2$ | $50 \times 40$ | 1.40 | 35.0 | 2.15 | 53.8 | 7.10 | 177.5 |
| $2-1 / 2 \times 1 / 2$ | $65 \times 15$ | 1.45 | 36.3 | 2.50 | 62.5 | 7.90 | 197.5 |
| $2-1 / 2 \times 3 / 4$ | $65 \times 20$ | 1.45 | 36.3 | 2.50 | 62.5 | 7.90 | 197.5 |
| $2-1 / 2 \times 1$ | $65 \times 25$ | 1.45 | 36.3 | 2.50 | 62.5 | 7.90 | 197.5 |
| 2-1/2 $\times 1-1 / 4$ | $65 \times 32$ | 1.45 | 36.3 | 2.50 | 62.5 | 7.90 | 197.5 |
| 2-1/2 $\times 1-1 / 2$ | $65 \times 40$ | 1.45 | 36.3 | 2.50 | 62.5 | 7.90 | 197.5 |
| $2-1 / 2 \times 2$ | $65 \times 50$ | 1.45 | 36.3 | 2.50 | 62.5 | 7.90 | 197.5 |
| $3 \times 1 / 2$ | $75 \times 15$ | 1.50 | 37.5 | 2.70 | 67.5 | 9.75 | 243.8 |
| $3 \times 3 / 4$ | $75 \times 20$ | 1.50 | 37.5 | 2.70 | 67.5 | 9.75 | 243.8 |
| $3 \times 1$ | $75 \times 25$ | 1.50 | 37.5 | 2.70 | 67.5 | 9.75 | 243.8 |
| $3 \times 1-1 / 4$ | $75 \times 32$ | 1.50 | 37.5 | 2.70 | 67.5 | 9.75 | 243.8 |
| $3 \times 1-1 / 2$ | $75 \times 40$ | 1.50 | 37.5 | 2.70 | 67.5 | 9.75 | 243.8 |
| $3 \times 2$ | $75 \times 50$ | 1.50 | 37.5 | 2.70 | 67.5 | 9.75 | 243.8 |
| $4 \times 1 / 2$ | $100 \times 15$ | 1.56 | 39.0 | 3.10 | 77.5 | 10.17 | 254.3 |
| $4 \times 3 / 4$ | $100 \times 20$ | 1.56 | 39.0 | 3.10 | 77.5 | 10.17 | 254.3 |
| $4 \times 1$ | $100 \times 25$ | 1.56 | 39.0 | 3.10 | 77.5 | 10.17 | 254.3 |
| $4 \times 1-1 / 4$ | $100 \times 32$ | 1.56 | 39.0 | 3.10 | 77.5 | 10.17 | 254.3 |
| $4 \times 1-1 / 2$ | $100 \times 40$ | 1.56 | 39.0 | 3.10 | 77.5 | 10.17 | 254.3 |
| $4 \times 2$ | $100 \times 50$ | 1.56 | 39.0 | 3.10 | 77.5 | 10.17 | 254.3 |
| $6 \times 1 / 2$ | $150 \times 15$ | 1.80 | 45.0 | 3.96 | 99.0 | 13.00 | 325.0 |
| $6 \times 3 / 4$ | $150 \times 20$ | 1.80 | 45.0 | 3.96 | 99.0 | 13.00 | 325.0 |
| $6 \times 1$ | $150 \times 25$ | 1.80 | 45.0 | 3.96 | 99.0 | 13.00 | 325.0 |
| $6 \times 1-1 / 4$ | $150 \times 32$ | 1.80 | 45.0 | 3.96 | 99.0 | 13.00 | 325.0 |
| $6 \times 1-1 / 2$ | $150 \times 40$ | 1.80 | 45.0 | 3.96 | 99.0 | 13.00 | 325.0 |
| $6 \times 2$ | $150 \times 50$ | 1.80 | 45.0 | 3.96 | 99.0 | 13.00 | 325.0 |

CycleTough ${ }^{\oplus}$ Piping Systems contio

Reducing Tee - G x G x G

| SIZE |  | C |  | H |  | L |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm |
| $2 \times 1-1 / 2$ | $50 \times 40$ | 1.30 | 32.5 | 1.10 | 27.5 | 7.60 | 190.0 |
| $2-1 / 2 \times 2$ | $65 \times 50$ | 1.67 | 41.8 | 1.63 | 40.8 | 9.50 | 237.5 |
| $3 \times 1-1 / 2$ | $75 \times 40$ | 1.85 | 46.3 | 1.60 | 40.0 | 10.80 | 270.0 |
| $3 \times 2$ | $75 \times 50$ | 1.85 | 46.3 | 1.60 | 40.0 | 10.80 | 270.0 |
| $3 \times 2-1 / 2$ | $75 \times 65$ | 1.90 | 47.5 | 1.60 | 40.0 | 10.80 | 270.0 |
| $4 \times 2$ | $100 \times 50$ | 1.90 | 47.5 | 2.00 | 50.0 | 11.30 | 282.5 |
| $4 \times 2-1 / 2$ | $100 \times 65$ | 1.90 | 47.5 | 2.00 | 50.0 | 11.30 | 282.5 |
| $4 \times 3$ | $100 \times 75$ | 1.90 | 47.5 | 2.00 | 50.0 | 11.30 | 282.5 |
| $6 \times 2$ | $150 \times 50$ | 2.40 | 60.0 | 2.80 | 70.0 | 14.90 | 372.5 |
| $6 \times 2-1 / 2$ | $150 \times 65$ | 2.40 | 60.0 | 2.80 | 70.0 | 14.90 | 372.5 |
| $6 \times 3$ | $150 \times 75$ | 2.40 | 60.0 | 2.80 | 70.0 | 14.90 | 372.5 |
| $6 \times 4$ | $150 \times 100$ | 2.40 | 60.0 | 2.80 | 70.0 | 14.90 | 372.5 |
| $8 \times 2$ | $200 \times 50$ | 3.85 | 96.3 | 4.87 | 121.8 | 19.50 | 487.5 |
| $8 \times 3$ | $200 \times 75$ | 3.85 | 96.3 | 4.87 | 121.8 | 19.50 | 487.5 |
| $8 \times 4$ | $200 \times 100$ | 3.85 | 96.3 | 4.88 | 122.0 | 19.50 | 487.5 |
| $8 \times 6$ | $200 \times 150$ | 3.85 | 96.3 | 4.88 | 122.0 | 19.50 | 487.5 |



Cross GxGxGxG

| SIZE |  | C |  | H |  | L |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm |
| 4 | 100 | 4.00 | 100.0 | 4.00 | 100.0 | 12.50 | 312.5 |
| 6 | 150 | 4.50 | 112.5 | 4.50 | 112.5 | 16.00 | 400.0 |

Stop Coupling G x G

| SIZE |  | L |  | $D$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm |
| 2 | 50 | 5.00 | 125.0 | 3.35 | 83.8 |
| $2-1 / 2$ | 65 | 7.14 | 178.5 | 4.15 | 103.8 |
| 3 | 75 | 7.00 | 175.0 | 5.00 | 125.0 |
| 4 | 100 | 7.40 | 185.0 | 6.13 | 153.3 |
| 6 | 150 | 10.00 | 250.0 | 8.73 | 218.3 |
| 8 | 200 | 12.30 | 307.5 | 10.62 | 265.5 |

CycleTough ${ }^{\ominus}$ Piping Systems contio

Repair Coupling G x G

| SIZE |  | L |  | D |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm |
| 2 | 50 | 7.20 | 180.0 | 3.35 | 83.8 |
| $2-1 / 2$ | 65 | 7.00 | 175.0 | 4.15 | 103.8 |
| 3 | 75 | 7.00 | 175.0 | 5.00 | 125.0 |
| 4 | 100 | 7.40 | 185.0 | 6.13 | 153.3 |
| 6 | 150 | 10.00 | 250.0 | 8.73 | 218.3 |
| 8 | 200 | 12.30 | 307.5 | 10.62 | 265.5 |

Permanent Plug Spigot

| SIZE |  | L |  |
| :---: | :---: | :---: | :---: |
| in | mm | in | mm |
| $1-1 / 2$ | 40 | 2.50 | 62.5 |
| 2 | 50 | 2.50 | 62.5 |
| $2-1 / 2$ | 65 | 3.50 | 87.5 |
| 3 | 75 | 3.50 | 87.5 |
| 4 | 100 | 3.75 | 93.8 |
| 6 | 150 | 4.50 | 112.5 |

Increaser Bushing - G x Sp

| SIZE |  | L |  | C |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm |
| $1-1 / 2 \times 2$ | $40 \times 50$ | 2.40 | 60.0 | 0.20 | 5.0 |
| $2 \times 2-1 / 2$ | $50 \times 65$ | 2.40 | 60.0 | 0.20 | 5.0 |
| $2 \times 3$ | $50 \times 75$ | 3.40 | 85.0 | 0.55 | 13.8 |
| $2-1 / 2 \times 3$ | $65 \times 75$ | 3.40 | 85.0 | 0.38 | 9.5 |
| $2 \times 4$ | $50 \times 100$ | 3.00 | 75.0 | 0.40 | 10.0 |
| $2-1 / 2 \times 4$ | $65 \times 100$ | 3.00 | 75.0 | 0.40 | 10.0 |
| $3 \times 4$ | $75 \times 100$ | 3.00 | 75.0 | 0.40 | 10.0 |
| $2 \times 6$ | $50 \times 150$ | 4.30 | 107.5 | 0.50 | 12.5 |
| $2-1 / 2 \times 6$ | $65 \times 150$ | 4.30 | 107.5 | 0.50 | 12.5 |
| $3 \times 6$ | $75 \times 150$ | 4.30 | 107.5 | 0.50 | 12.5 |
| $4 \times 6$ | $100 \times 150$ | 4.30 | 107.5 | 0.50 | 12.5 |
| $4 \times 8$ | $100 \times 200$ | 5.10 | 127.5 | 0.60 | 15.0 |
| $6 \times 8$ | $150 \times 200$ | 5.10 | 127.5 | 0.60 | 15.0 |

## CycleTough ${ }^{\ominus}$ Piping Systems cont'o

Adapter - Flange x Gasket Bell


| SIZE |  | C |  | D |  | L |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm | in | mm |
| $1-1 / 2$ | 40 | 3.85 | 96.3 | 5.00 | 125.0 | 4.25 | 106.3 |
| 2 | 50 | 4.75 | 118.8 | 6.00 | 150.0 | 4.75 | 118.8 |
| $2-1 / 2$ | 65 | 5.50 | 137.5 | 7.00 | 175.0 | 5.75 | 143.8 |
| 3 | 75 | 6.00 | 150.0 | 7.50 | 187.5 | 6.50 | 162.5 |
| 4 | 100 | 7.48 | 187.0 | 9.02 | 225.5 | 10.52 | 263.0 |
| 6 | 150 | 9.55 | 238.8 | 10.97 | 274.3 | 13.48 | 337.0 |
| 8 | 200 | 11.75 | 293.8 | 13.50 | 337.5 | 12.00 | 300.0 |

Spigot Adapter G x Sp


| SIZE |  | L |  |
| :---: | :---: | :---: | :---: |
| in | mm | in | mm |
| $1-1 / 2$ | 40 | 1.50 | 37.5 |
| 2 | 50 | 1.80 | 45.0 |
| $2-1 / 2$ | 65 | 2.00 | 50.0 |
| 3 | 75 | 2.10 | 52.5 |
| 4 | 100 | 2.30 | 57.5 |
| 6 | 150 | 3.10 | 77.5 |

## Male Adapter G x Male Pipe Thread

| SIZE |  | L |  |
| :---: | :---: | :---: | :---: |
| in | mm | in | mm |
| $1-1 / 2$ | 40 | 1.05 | 26.3 |
| 2 | 50 | 1.20 | 30.0 |
| $2-1 / 2$ | 65 | 1.55 | 38.8 |
| 3 | 75 | 2.10 | 52.5 |
| 4 | 100 | 2.25 | 56.3 |
| 6 | 150 | 2.50 | 62.5 |



## CycleTough ${ }^{\oplus}$ Piping Systems cont'o

| SIZE |  |  |  |
| :---: | :---: | :---: | :---: |
| in | mm | L |  |
| $1-1 / 2$ | 40 | in | mm |
| 2 | 50 | 2.60 | 65.0 |
| $2-1 / 2$ | 65 | 3.00 | 75.0 |
| 3 | 75 | 3.80 | 95.0 |
| 4 | 100 | 4.10 | 102.5 |
| 6 | 150 | 4.40 | 110.0 |

Adapter - PE (Plain End) x Male Pipe Thread


| SIZE |  | L |  | C |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| in | mm | in | mm | in | mm |
| 3 | 75 | 4.30 | 107.5 | 2.00 | 50.0 |
| 4 | 100 | 4.40 | 110.0 | 2.25 | 56.3 |
| 6 | 150 | 5.90 | 147.5 | 2.50 | 62.5 |

## TerraBrute ${ }^{\oplus}$ Restrained Joint Pipe

TerraBrute is a modified AWWA C900 pipe that has been specifically designed for use with trenchless installation techniques like horizontal directional drilling (HDD) and pipe bursting. Using an innovative system of rings and pins, TerraBrute can withstand higher pull forces than any other plastic piping system, while simultaneously being able to bend and flex in a borehole.

In addition to trenchless installations, TerraBrute's versatile joint is perfect for above ground installations like bridge crossings where there may be significant temperature extremes. Where other piping systems require costly and maintenance intensive expansion joints, the wide groove in each TerraBrute joint allows expansion and contraction of each pipe.
Another key attribute of the TerraBrute joint is that it allows pipe rotation without damage. This can be an issue in seismic zones where piping systems are subjected to a wide variety of soil induced stresses during earthquake events.


## Applications:

HDD, pipe bursting, bridge crossings, seismic zones, casing installations and steep slopes.


## TerraBrute ${ }^{\oplus}$ Restrained Joint Pipe conr'o

## Pulling Forces

The magnitude of pulling force exerted on a pipe string during pulled in place type installation methods depends on a number of factors, including:

- The length of the pull
- The diameter of the pipe
- The type of soil
- Selection of drilling fluid.

TerraBrute has been designed to withstand extremely high pulling forces in order to perform under even the toughest conditions. While most projects will use only a fraction of the ultimate strength of TerraBrute, the extra strength acts as an "insurance policy" against unexpected conditions.

TerraBrute's ultimate pull strength has been verified by laboratory tests, and can be calculated using a semiempirical design method derived by researchers at the University of Western Ontario (UWO). The following table shows both the ultimate pulling capacity of the product (no safety factor) as well as the recommended maximum pulling capacity (2:1 safety factor)

| Nominal Size |  | Recommended <br> Pulling Limit |  | Ultimate Pulling <br> Capacity <br> (Straight Pull) |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| mm | Inches | kN | Ibs | kN | Lbs. |
| 100 | 4 | 50 | 11200 | 100 | 22400 |
| 150 | 6 | 110 | 24700 | 220 | 49500 |
| 200 | 8 | 115 | 25800 | 230 | 51700 |
| 250 | 10 | 187 | 42100 | 375 | 84300 |
| 300 | 12 | 275 | 61800 | 550 | 123600 |

## Bending Forces

PVC pipe is much stiffer than the pipe material most commonly used for HDD and other trenchless methods - HDPE pipe. This has led some designers to wonder if PVC is too rigid to be used for these types of applications. In fact, stiffness and flexibility are two different properties. It is possible for a material to be very stiff and strong but still quite flexible. TerraBrute is flexible enough for virtually any HDD or pipe bursting operation, and can be installed to a much tighter radius than other PVC products. In fact, since TerraBrute is more flexible than the drilling rods, there is virtually no way to "over bend" the pipe. In addition, the high stiffness of the material means that there is very little deformation of the pipe string during pulling operations. As a result, appurtenances such as services and hydrant leads can be installed immediately after pulling operations are completed.

One of the most important characteristics of the TerraBrute joint is that it allows significant joint deflection. A significant portion of the bending is taken up by the joints, which reduces the amount of stress exerted on the pipe ball from bending. This allows TerraBrute to be installed to a much tighter radius than other PVC products.
The table below shows how much TerraBrute can be deflected at the joint during pullback operations, as well as how much the pipe barrel itself can be bent. Most projects will involve both pipe bending and joint deflection, often at the same time.

| Nominal <br> Size |  | Allowable Joint <br> Deflection | Allowable Pipe <br> Bending | Minimum <br> Allowable Radius |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| mm | in | (degrees) | (degrees) | meters | Feet |
| 100 | 4 | 8.5 | 5.7 | 11.3 | 37.1 |
| 150 | 6 | 8.5 | 4 | 13.1 | 43 |
| 200 | 8 | 7.5 | 3 | 15.9 | 52.2 |
| 250 | 10 | 5 | 2.5 | 22.8 | 74.8 |
| 300 | 12 | 5 | 2.1 | 24.1 | 79.1 |



TerraBrute ${ }^{\oplus}$ Restrained Joint Pipe cont'o


## TerraBrute ${ }^{\oplus}$ Restrained Joint Pipe cont’d

## External Pressures

Drilling fluids are used under many different soil conditions both to keep the borehole open and to remove the spoil from drilling and reaming operations. This drilling fluid is pressurized, and as a result, it is important that a pipe joint be able to withstand these external pressures without leaking fluid into the pipe string. IPEX has tested fully deflected joints to well over 100 psi external pressure with zero leakage.

## Standards

AWWA C900
TerraBrute is made with pipe conforming to AWWA C900, however once the pipe is grooved on the spigot end its dimensions do not match those published in the C900 standard. Because of this small dimensional difference the pipe, once grooved, does not strictly conform to the C900 standard. It is important to note however, that TerraBrute is subjected to the same testing program as IPEX's Blue Brute (C900) pipe.
CSA B137.3
TerraBrute is made from stock certified to CSA B137.3.
NQ 3624-250

## Factory Mutual and Underwriter's Laboratories

TerraBrute is made from starting stock that is Factory Mutual, ULC and ULI Approved


## Short Form Specifications

PVC Pipe used for horizontal directional drilling (HDD) or other trenchless installation methods shall be manufactured with a cast iron outside diameter (CIOD) and shall be made with starting stock meeting the requirements of AWWA C900 for $100 \mathrm{~mm}-300 \mathrm{~mm}$ (4" - 12") diameters. Starting stock will also be certified to CSA B137.3, must be Factory Mutual approved, and listed by ULC and ULI.
The maximum allowable pulling force shall be the ultimate tensile capacity of the piping system divided by a safety factor of 2 , as shown in the table below.

| Nominal Size |  | Maximum Allowable <br> Pulling Force |  |
| :---: | :---: | :---: | :---: |
| mm | Inches | kN | Lbs. |
| 100 | 4 | 50 | 11200 |
| 150 | 6 | 110 | 24700 |
| 200 | 8 | 115 | 25800 |
| 250 | 10 | 187 | 42100 |
| 300 | 12 | 275 | 61800 |

PVC pipe must be manufactured with an integral bell, and must have removable gaskets to allow the use of oil-resistant (nitrile) gaskets in contaminated soils.

## Dimensions

TerraBrute is virtually identical to Blue Brute dimensionally. It has a slightly shorter laying length, 6.0 meters (19'8") as a result of the slightly extended bell, as well as a groove cut into the spigot end of the pipe. One key dimension that must be remembered when planning pre-ream operations is the absolute maximum outside diameter of the pipe. The table below shows the maximum outside diameter of each size.

| Nominal Size |  | Maximum Outside Diameter <br> (Outside Ring) |  |
| :---: | :---: | :---: | :---: |
| mm | Inches | mm | Inches |
| 100 | 4 | 160 | 6.3 |
| 150 | 6 | 230 | 9.1 |
| 200 | 8 | 290 | 11.4 |
| 250 | 10 | 350 | 14.2 |
| 300 | 12 | 415 | 16.3 |

Due to the extended bell configuration, TerraBrute has slightly shorter laying length than standard Blue Brute pipe:

| Nominal Size |  | Laying Lengths |  |
| :---: | :---: | :---: | :---: |
| mm | Inches | m | Feet/Inches |
| 100 | 4 | 6.04 | $19^{\prime} 10^{\prime \prime}$ |
| 150 | 6 | 6.03 | $19^{\prime} 9{ }^{\prime \prime}$ |
| 200 | 8 | 6.01 | $19^{\prime} 9{ }^{\prime \prime}$ |
| 250 | 10 | 6.01 | $19^{\prime} 9{ }^{\prime \prime}$ |
| 300 | 12 | 6.01 | $19^{\prime} 9{ }^{\prime \prime}$ |

## Standards for PVC Pressure Systems

## Standards and Certification

There are two main classes of standards governing PVC piping systems, those which define products that are certified by a third party and those which define products that are non-policed. While non-policed standards can be very useful in a specification, the standards that are certified by a third party offer the customer an additional level of quality assurance. Third party certification means that an independent organization has scrutinized the manufacturing process and QA/QC procedures for the products in question, and has verified that they meet the minimum requirements for approval. Compliance with a non-policed standard requires the customer to take the manufacturer at his word that his product conforms to the standard. Most manufacturers perform accurate in house testing and are honest and up front, and if when they state that their products meet a certain standard, you can be quite certain that they do. There is no question however, that certification by a third party provides a much higher degree of assurance that the products in question in fact meets the applicable standard and that it will perform as stated.

## Third Party Certified Standards

## Canadian Standards Association (CSA)

CSA B137.0
CSA B137.1
CSA B137.2
CSA B137.3
CSA B137.9
CSA Staff visit all IPEX plants producing certified product several times each year. In addition to witnessing manufacturing and QA/QC procedures, CSA staff also inspect records, and select product samples for independent testing. The CSA standards refer to a wide variety of external standards (such as ASTM standards) for such things as testing methods. As a result, certifying the product to a CSA standard often has the effect of indirectly certifying the product to other standards as well.

## Factory Mutual and Underwriter's Laboratories

FM 1612
UL and ULI Listed to Standard 1285
These third party certified standards are often required whenever the piping system is going to be used as a fire protection line. Insurance regulations often dictate the required standard, however to be safe, most designers simply specify all three CSA, UL and FM organizations. The certification methods are similar to those used by the CSA plant inspections and independent material testing.

## National Sanitation Foundation (NSF)

NSF-61
NSF-14
NSF 61 certification is required for all products that will carry potable water. NSF 14 standards do not deal with product performance, including but with the effect of the product on potable water. NSF certification means that the compound used to make the pipe or fitting has no adverse effect on the water it carries. NSF certifies the material, not the pipe or fitting itself.

## Accreditation of Standards Labs and Organizations

While the standards discussed above are normally certified by a third party, that third party can sometimes be a separate organization. For example, Intertek Warnock-Hersey is a laboratory accredited by the Standards Council of Canada, and as a result, it is capable of certifying products to standards. It is common for Intertek Warnock-Hersey to certify a product to a CSA standard, and NSF also has this capability.

Only NSF, FM and UL can certify to their own standards however.

## Non-Certified Standards

American Water Works Association
AWWA C900
AWWA C903
AWWA C905

## AWWA C907

C900, 905 and 907 all deal with PVC pressure pipe and fittings, while C903 is a new standard for composite service piping. Q-line is covered by this standard. AWWA standards are most commonly used when specifying piping systems for water transmission or distribution.

## ASTM Standards (Various standards)

ASTM Standards are referenced by all the above standards. They cover everything from manufacturing to testing and installation, which is why there are so many different ASTM standards associated with our products. While they are "nonpoliced", the fact that many ASTM standards are included in policed standards means that indirectly, they are third party certified standards.

## Design and Installation Standards

AWWA M23 - PVC Pipe - Design and Installation The M23 manual sets out all of the guidelines needed to properly design and install a PVC water system. In addition, it carefully defines the difference between distribution mains and transmission mains, and explains how to properly design for surges. It also includes worked examples of the various design concepts. It is an excellent reference for anyone involved with water system design or installation.

## Section 2: Properties of PVC Pressure Pipe and Pressure System Design

## Introduction

Properly designed and installed PVC piping systems will last virtually forever. Recent research has unearthed PVC systems that were installed in the 1930's that exhibit virtually no reduction in serviceability. This section focuses on the physical properties of PVC pipes and fittings, as well as how to approach some of the conditions likely to be encountered during a project.
Various design issues will also be addressed including;

- The hydrostatic design basis (HDB) of PVC pipe
- Calculating pressure ratings
- Hydraulics and headloss calculations
- Restraint design
- Installation in contaminated soils
- Surge pressures in PVC pipe
- Air entrapment and proper location of air release valves
- Thermal effects
- Design for cyclic fatigue


## Material Properties of PVC

## Design Life

Designers should use a minimum 100 year design life when carrying out lifecycle costing calculations for PVC systems. This is backed up both by research and real world installations.

## Current Research

PVC pressure pipes have been in service for over 70 years in Europe ${ }^{2}$. Samples of 70 year old pipe have been excavated and have exhibited no reduction in serviceability. PVC pipe's installed history in North America is approaching 50 years, with a similar record for flawless service. The single most destructive force attacking our municipal water and sewer infrastructure is corrosion. By using materials that are immune to electrolytic corrosion or chemical attack, designers eliminate the single most common problem associated with buried infrastructure.

Research dealing with the longevity of PVC pipe in various conditions is on-going, however there have been a number of notable research papers presented over the years, including:

- AWWA Research Foundation - "Quantifying Future Rehabilitation and Replacement Needs of Watermains", 1998

This study used a highly specialized computer model to estimate the life of various materials based on past performance. In the one North American City studied with a significant amount of PVC pipe installed, PVC was rated at a minimum 100 years while concrete and ductile iron were rated at 85 and 60 years respectively.

- "PVC Pipe Study - Performance of PVC Water Main

Pipe installed in the City of Edmonton between 1977 and 1994".

A comprehensive study of PVC pipe used in the City's water distribution system rated its service life at a minimum of 88 years with minimal maintenance.

## Case Studies from Europe and North America including:

- Dallas, Texas - A PVC sewer pipe installed in 1973 was excavated and subjected to each of the tests outlined in ASTM D3034. The results show that the excavated pipe still met all the standards applicable to new pipe
- Denmark - A PVC Sewer pipe installed in 1963 was excavated and testing results show that the pipe has the same material properties as newly produced pipe. Most of the pipes installed were directly into native soil without bedding, and have performed acceptably for over 40 years.

These research papers are available upon request from your IPEX marketing representative at marketing@ipexinc.com or visit the IPEX website at www.ipexinc.com.


[^1]
## Design Strength

While Blue Brute pipes are casually referred to as PVC pipes, in reality they are made of a special PVC compound designed specifically for use in piping systems. The Hydrostatic design basis (HDB) of a PVC compound is the minimum stress that the material is able to withstand over a given time. The HDB's of IPEX compounds are established through both short-term and long-term testing (up to 100,000 hours sustained pressure). By plotting the results on a logarithmic scale, the 50 or 100 year design stresses can be easily extrapolated. The diagram below shows a typical life line for a PVC compound.

Figure 1 - Stress Regression Line - 12454

Table 3 - Summary of Properties

| Material Property |  |
| :--- | :---: |
| Long-term Hydrostatic Design Basis <br> (HDB) | $26.6 \mathrm{MPa}(4000 \mathrm{psi})$ |
| Short-Term Hydrostatic Design Basis <br> (STHDB) | $44.1 \mathrm{Mpa}(6400 \mathrm{psi})$ |
| ASTM Cell Class (ASTM F1784) | 12454 B |
| Young's Modulus | $266 \mathrm{Mpa}(400,000 \mathrm{psi})$ |
| Poisson's Ratio | 0.38 |

## Chemical Permeation and Installation of PVC Pipe in Contaminated Soils

There is a misconception among some designers that PVC pipe is unsuitable for installation in areas that contain soils contaminated by organic compounds. This misconception stems from the fact that there have been rare occurrences where small diameter plastic service lines have been permeated by organic chemicals. This is not an issue with larger diameter PVC pipes because:

1. The vast majority of documented permeation incidents occurred with thin wall service pipes made of lower density materials such as polybutylene or polyethylene ${ }^{3}$. These small diameter pipes are indeed unsuitable for contaminated soils. Only service pipe with a built in permeation barrier (such as Q-Line) should be used in these cases.
2. PVC pipe has an effective permeation time of many centuries, even at extremely high levels of environmental contamination. This has been conclusively proven through research ${ }^{4}$.
3. The high density and non-porous finish of PVC pipe makes it very difficult for permeation to occur. Samples of IPEX pressure pipe we partially filled with gasoline and sealed for seven years. When the inside surface of the pipe was examined microscopically, no evidence of permeation was found ${ }^{5}$.

Gaskets are the weak link when installing gasketed piping systems in contaminated soils, the most important consideration is the gasket material, regardless of the piping material. To ensure safe, long-term operation of the pipeline, oil-resistant (nitrile) gaskets should always be specified.

Lastly, many designers consult chemical resistance guides for information about installation in contaminated soils. These guides are usually inappropriate for this application as they typically deal with a $100 \%$ concentration of the material in question. You should consult with your IPEX technical representative before making any decisions with respect to suitability for a particular application.

## Thermal Effects and UV Resistance

PVC pipe can become discolored when exposed to direct sunlight for a long period of time. This discoloration affects only the surface of the material (to a depth of 0.001 and 0.003 inches), and does not appreciably affect the performance of the pipe. A slight reduction in the impact strength of the pipe occurs, while the tensile strength and the modulus of elasticity are unaffected. If gasketed PVC pressure piping will be used in an exposed location, painting the surface of the pipe with a latex based paint, or covering it with an opaque barrier will eliminate the effects of U.V. exposure.
The vast majority of gasketed pressure piping is installed underground, eliminating the issue of UV exposure.

PVC is a thermoplastic, which means its mechanical properties change with temperature. The pressure rating for PVC pipe (and most other thermoplastic piping materials) is calculated at $23^{\circ} \mathrm{C}\left(73^{\circ} \mathrm{F}\right)$. Above that temperature, the tensile strength of the material decreases, and the pressure rating must be de-rated by the factors shown in the table below. The maximum recommended service temperature for PVC pressure pipe is $140^{\circ} \mathrm{F}$.

Table 4 - Temperature Effects on PVC Pressure Pipe

| ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | Multiply the pressure <br> rating by these factors |
| :---: | :---: | :---: |
| 32 | 90 | 0.75 |
| 38 | 100 | 0.62 |
| 43 | 110 | 0.50 |
| 49 | 120 | 0.40 |
| 54 | 130 | 0.30 |
| 60 | 140 | 0.22 |

## Expansion and Contraction

While buried applications seldom involve significant temperature variations, applications such as bridge crossings or casing installations can have temperature variations. When considering the use of unrestrained joints or TerraBrute joints, expansion and contraction should be calculated per length of pipe. If the joints are restrained using conventional restrainers, or a solvent cemented joint is used, expansion and contraction should be calculated using the full length of restrained pipe.

| Material | Coefficient <br> in/in/ $/ \mathrm{F}$ | Expansion <br> $\mathrm{in} / 100 \mathrm{ft} / 10^{\circ} \mathrm{F}$ | Coefficient <br> $\mathrm{mm} / \mathrm{mm} /{ }^{\circ} \mathrm{C}$ | Expansion <br> $\mathrm{mm} / 10 \mathrm{~m} / 10^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: |
| PVC | $3.0 \times 10^{-5}$ | 0.36 | $5.4 \times 10^{-5}$ | 5.4 |
| HDPE | $1.2 \times 10^{-4}$ | 1.44 | $1.4 \times 10^{-4}$ | 21.6 |
| Ductile Iron | $6.2 \times 10^{-6}$ | 0.07 | $1.1 \times 10^{-5}$ | 1.1 |
| Concrete | $5.5 \times 10^{-6}$ | 0.07 | $9.9 \times 10^{-6}$ | 1.0 |
| Steel | $6.5 \times 10^{-6}$ | 0.08 | $1.2 \times 10^{-5}$ | 1.2 |

## Design Calculations

## How to Calculate a Pressure Class or Pressure Rating

The ISO Equation for thermoplastics makes calculating required dimension ratios and pressure ratings very simple.

While it is referred to as the ISO Equation, it was actually developed in 1852, for use with all sorts of pressure vessels, and has been used ever since. The derivation is simple:
Referring to the Figure, we can see that the force in the pipe wall is:
Force $=\left(\frac{\mathrm{P}_{\mathrm{i}} \mathrm{D}}{2}\right)$

Therefore, the maximum stress in the pipe wall is:

$$
\begin{aligned}
\sigma_{\max } & =\frac{P_{i} \overline{\mathrm{D}}}{2 \mathrm{t}} \text {, where } \overline{\mathrm{D}}=\text { the average diameter of the pipe } \\
\overline{\mathrm{D}} & =\text { Do }-\mathrm{t} \therefore \sigma_{\max }=\frac{P_{i}(\mathrm{Do}-\mathrm{t})}{2 \mathrm{t}}
\end{aligned}
$$

But since $\mathrm{DR}=\frac{\mathrm{Do}}{\mathrm{t}}$, then $\sigma_{\max }=\frac{\mathrm{P}_{1}(\mathrm{DR}-1)}{2}$
The conservative design procedure of PVC pipe requires that a safety factor be applied to the hydrostatic design basis in order to arrive at a design stress $-S$. This design stress then becomes the maximum allowable stress in the material. Note that the short and long term strengths of the material are different, therefore the short-term design stress and the longterm design stress will be different.
The safety factor is usually set between 2 and 2.5 depending on the application, and the standard governing the design.

$$
\mathrm{S}=\frac{\sigma_{\mathrm{max}}}{\mathrm{SF}}
$$

Substituting this expression for design stress, we get

$$
\mathrm{S}=\frac{\mathrm{P}(\mathrm{DR}-1)}{2} \therefore \mathrm{P}=\frac{2 \mathrm{~S}}{(\mathrm{DR}-1)}
$$

This form of the equation allows the pressure capabilities of a given dimension ratio to be quickly and easily calculated. To see a worked example of how to calculate pressure ratings, please refer to section 3.

## Calculating a Pressure Rating

There are two ratings on every PVC pipe - a long term pressure rating (LTR) which is used for evaluating working pressure capacity, and a short term pressure rating (STR) designed for evaluating surge and transient pressure capability.

To calculate an STR, simply apply the ISO equation using the short term HDB.

Recall that:

$$
\mathrm{S}=\frac{\sigma_{\max }}{\mathrm{SF}}
$$

For short term stresses, AWWA M23 sets the safety factor $(S F)=2.5$. Using the short term HDB gives:
$\mathrm{S}_{\mathrm{str}}=\frac{6400}{2.5}=2560 \mathrm{psi}$
Therefore for DR41 pipe, the STR is given by
$\mathrm{STR}=\frac{2(2560)}{(41-1)}=128 \mathrm{psi}$
For long term stresses, the safety factor is set at 2.0:
$S_{\mathrm{tr}}=\frac{4000}{2}=2000 \mathrm{psi}$
Applying the ISO Equation:
$\operatorname{LTR}=\frac{2(2000)}{(41-1)}=100 \mathrm{psi}$
The table below shows both the LTR and the STR for various thicknesses of PVC pipe

| SDR | Short Term Rating <br> STR* (2.5:1 S.F.) $_{(\mathrm{psi})}$ | Long Term Rating <br> LTR* (2:1 S.F.) <br> (psi) |
| :---: | :---: | :---: |
| 51 | 100 | 80 |
| 41 | 130 | 100 |
| 32.5 | 165 | 125 |
| 26 | 205 | 160 |
| 25 | 215 | 165 |
| 18 | 300 | 235 |
| 14 | 395 | 305 |

[^2]
## Calculating a Pressure Class as per AWWA C900 (100mm - 300mm CIOD Pipe)

The C900 standard refers to Pressure Classes, which are different from pressure ratings. A pressure class differs from a pressure rating in a number of ways:

It includes a design safety factor (F) of 2.5 as opposed to 2.0
It includes a "surge allowance" equivalent to the pressure generated by a theoretical instantaneous stoppage of $0.6 \mathrm{~m} / \mathrm{s}$ ( $2 \mathrm{ft} / \mathrm{s}$ ) in the pipeline

The short term pressure class is not used as a $2 \mathrm{ft} / \mathrm{s}$ ( 0.6 $\mathrm{m} / \mathrm{s}$ ) surge is already included
$\mathrm{PC}=\left[\frac{(2 \times \mathrm{HDB})}{(\mathrm{DR}-1)} \times \frac{1}{\mathrm{~F}}\right]-\mathrm{P}_{\mathrm{s}}$
$\mathrm{PC}=\left[\frac{2(4000)}{(\mathrm{DR}-1)} \times \frac{1}{2.5}\right]-\mathrm{P}_{\mathrm{S}}$

Table 5 - AWWA C900 Pressure Classes (100mm-300mm (4"-12") pipe)

| Dimension Ratio | Ps $=0.6 \mathrm{~m} / \mathrm{s}(2 \mathrm{ft} / \mathrm{s})$ <br> $(\mathrm{psi})$ | Pressure Class |
| :---: | :---: | :---: |
| 25 | 30 | 100 |
| 18 | 35 | 150 |
| 14 | 40 | 200 |

## Calculating Friction Headloss in PVC Piping Systems

One of the advantages in using PVC pipe is that its smooth inside finish dramatically reduces friction headloss when compared to other materials. As a result, pumping costs are lower and flows are higher when considering the same nominal diameter between materials.

The Hazen-Williams equation is one of the most commonly used methods for calculating friction headloss in a pipeline. It allows the friction headloss to be easily calculated for any piping system using flow coefficients that reflect the roughness of the piping material. Research has established that the Hazen-Williams flow coefficient for PVC pipe can vary between 155 to 165 for both new and previously used PVC pipe ${ }^{6}$. Therefore, a conservative coefficient of 150 is appropriate for all design situations. This value is also recommended by the AWWA M23 Design Manual.

$$
\begin{array}{rll}
\mathrm{V} & =1.318 \mathrm{Cr}^{0.63} \mathrm{~S}^{0.54} & \\
\text { in USCS Units } \\
\mathrm{V} & =0.8492 \mathrm{Cr}^{0.63} S^{0.54} & \\
\text { in SI Units }
\end{array}
$$

[^3]Where:
$\mathrm{V}=$ average pipe velocity, $\mathrm{ft} / \mathrm{s}(\mathrm{m} / \mathrm{s})$
C $=$ Hazen-Williams Friction factor (150 for PVC Pipe)
$\mathrm{R}=$ Hydraulic radius ( $\mathrm{D} / 4$ for a full pipe), ft (m)
$\mathrm{S}=$ Hydraulic gradient or frictional head loss per unit length of pipe, $\mathrm{ft} / \mathrm{ft}$, ( $\mathrm{m} / \mathrm{m}$ )

## Comparing Headloss Among Various Piping Materials

For any given nominal diameter of pipe, there are two factors which will largely dictate the headloss per unit length:

1. Internal diameter - It is the internal diameter of the pipe that should be used for hydraulic calculations, not the nominal diameter. A larger internal diameter promotes a higher fluid flow and therefore a lower headloss.
2. Internal friction coefficient - While internal diameter is important, the influence of the pipeline's internal finish should not be neglected. While PVC and other plastics can sustain a smooth inside surface indefinitely, other materials tend to become rougher as a result of corrosion by-products forming over the long term. As a result, older iron pipes have been shown to have friction factors less than 100.

While experimental data has shown that the " C " factor can be as high as $155-165$ for both new and used PVC pipe, AWWA M23 Manual recommends a "C" factor of 150 for PVC".

## Table 6 - Hazen-Williams "C"-Factors ${ }^{8}$

| Material | "C" Factor |
| :---: | :---: |
| Plastic (PVC \& HDPE) | 150 |
| Iron (new) | 130 |
| Iron (20 yrs old) | 100 |

The " C " factors obviously have a significant effect on flow rates. Comparing various materials it can be seen that PVC pipe has a much lower headloss at any given flow than other common piping materials.

Class 52 iron pipe has a slightly higher inside diameter than DR18 PVC, but its low long-term C factor of 100 or less results in poor flow characteristics.

SDR9 HDPE has a high C factor of 150 , however it has a much thicker pipe wall and thus has a much lower inside diameter than PVC SDR18.

Figure 2 - Pipe Material
Headloss - 200 mm Pipe at $25 \mathrm{~L} / \mathrm{s}$


## Calculating Surge Pressures

Surge pressures (water hammer) are generated in a piping system whenever the fluid flowing in that system changes velocity. These changes in velocity can be caused by many things, including:

- The operation of valves and pumps
- Entrapped air being expelled
- Changes in demand

There are two main types of surge pressures - transient surges that occur as the system moves from one steady state condition to another (ie: the closing of a single valve), and cyclic surges, that occur as part of the normal operation of some types of pipelines. A good example of this is a sewage forcemain, where a pump is activated each time the level in a wet well reaches a certain point.

The magnitude of pressure surges is dependent upon a number of things, including the type of fluid being pumped, the magnitude of the velocity change, and also the type of pipe material. Rigid piping materials typically generate much higher surge pressures than flexible systems, which are able to absorb much more of the shock generated by a surge. In addition, the high short term strength of PVC allows it to have a much higher safety factor against short term pressures than other piping materials .
The calculation of transient effects in a large piping system (regardless of the piping material) is a complicated procedure requiring considerable expertise. Fortunately, there are many engineering firms that are highly qualified to undertake this type of analysis. IPEX has worked closely with some of these experts, and we would be happy to refer interested designers to them. We highly recommend that detailed transient analysis be carried out of all systems, particularly large diameter systems.

While a detailed analysis can be beneficial, it is possible to calculate the magnitude of individual surges in a pipeline using the elastic wave theory of surge analysis. The magnitude of the surge pressure caused by a rapidly closing valve, for example, is related to the rate of change of the flow, while the rate of travel of the pressure wave is related to the speed of sound in the fluid (modified by the piping material).

[^4]
## Calculating Wave Velocity

$$
a=\frac{4,660}{\sqrt{1+\mathrm{k} / \mathrm{E}(\mathrm{DR}-2)}}
$$

Where:
$\mathrm{A}=$ Wave velocity, ft/s
$\mathbf{K}=$ Bulk fluid modulus (300,000 psi for water)
$\mathrm{E}=\begin{aligned} & \text { Modulus of Elasticity for the pipe (400,000 psi } \\ & \text { for PVC) }\end{aligned}$

Once the wave speed has been calculated, the maximum pressure surge can be calculated using the equation:

$$
\mathrm{P}=\mathrm{a}(\Delta V)
$$

Where:

$$
\begin{aligned}
\mathrm{A} & =\text { wavespeed (ft/s) } \\
\Delta \mathrm{A} & =\text { maximum velocity change }(\mathrm{ft} / \mathrm{s}) \\
\mathbf{g} & =\text { acceleration due to gravity }\left(32.2 \mathrm{ft} / \mathrm{s}^{2}\right) \\
\mathrm{P} & =\text { maximum pressure surge }(\mathrm{psi})
\end{aligned}
$$

Applying the equations to all SDR's of PVC pipe, assuming a $1 \mathrm{ft} / \mathrm{s}(0.3 \mathrm{~m} / \mathrm{s})$ stoppage, gives the results in the table below:

| SDR | Surge Pressure (psi) |
| :---: | :---: |
| 51 | 10.8 |
| 41 | 11.4 |
| 32.5 | 12.8 |
| 26 | 14.5 |
| 25 | 14.7 |
| 18 | 17.4 |
| 14 | 19.8 |

## Vacuum Pressures

While pipe joints are tested to -10.8 psi to meet CSA Standards, IPEX has simulated negative pressures far in excess of full vacuum ( -14.7 psi). By applying external pressures in excess of 100 psi. This proves conclusively that IPEX pipe joints can easily withstand full vacuum pressures.

## Air Entrapment in Pipelines

Air in pipelines can cause significant difficulties in any pipeline system, and should be avoided wherever possible. This can be accomplished by careful design of the pump or gravity inlet, employing proper filling and testing procedures, laying the pipe to grade wherever possible and by properly siting and sizing air release valves.

Some of the problems caused by air entrapment include:

1. Air pockets can reduce the amount of cross sectional area available for fluid flow in at some points in the pipeline. This can result in higher headloss and fluctuations in flow rates caused by air movement
2. Flow fluctuations can cause surge pressures in the pipeline
3. Release or venting of the air can cause extremely high surge pressures.

## Sources of Air in Pipelines

The most common air sources are:

- Entrapment of air during filling operations
- Entrapment at the pump or gravity inlet
- Release of dissolved air from the fluid in the pipeline
- Air intake from air release valves


## Problems Associated with Air Entrapment

The key problem with air entrapment is that at some point the air may be vented in an uncontrolled way. As an air pocket travels along a pipeline, it may reach an area where it can be vented. This could be at an air release valve (good) or perhaps at a gasketed joint (bad). The gasketing systems in most pipelines are designed to work with water, not air. While in most cases the gasket will hold back a high pressure air pocket, at some point the gasket may be blown out of the joint, causing a rapid release of air. Since the air can be vented extremely quickly, the air pocket collapses at an extremely high rate. The water surges toward the orifice created by the blown gasket, but cannot be expelled at the same velocity as the air due to its much higher density. The result is a rapid deceleration of the flow and a huge transient shock wave sometimes at a magnitude that can cause pipe failure.

## Air Release Valves

Air release valves are designed to exhaust air under various different pressure conditions in the pipeline, while restricting the flow of liquid. Air release valves are different than Air/Vacuum release valves in that Air/Vacuum release valves have a much larger orifice and are designed to exhaust or intake very large volumes of air, such as during the filling or draining process. The orifice size for an air release valve is generally between $1 / 16^{\prime \prime}$ and $1 / 4$ " diameter, while air/vacuum release valves can be between 1 " and 8 ".

A third type of valve combines the two functions, and is called a combination air/vacuum release valve. It contains both a large and a small orifice, the larger being open during filling and draining operations, and the smaller being open continuously to exhaust any air that might collect during normal operation of a pipeline.

Automatic air release valves with a riser diameter to main pipe ratio, $d / D$, in the order of 0.01 should be used when untrained personnel fill or test the pipeline. Air release valves in this size range tend to limit the passage of air and allow time for the water to slow down before reaching the vent.
Hydrants are not useful for the venting of air from pipelines. The reason is that hydrant leads typically are located at the 3 o'clock or 9 o'clock position on a pipeline. Air vents must be located at high points (ie at 12 o'clock) to be effective.

## Pipeline Testing and Air Entrapment

The initial filling and testing of a pipeline is one of the most critical events in the lifetime of a pipeline system. The reason is that the potential for air entrapment is highest during this period. As a result, Design Engineers should include details and procedures covering filling and testing in their project specifications:

1. Pipelines should be installed at a grade which results in a minimum of high points. Abrupt transitions and sharp peaks should be avoided.
2. Automatic air and vacuum release valves should be properly sized and installed at all high points or other areas where air could be expected to accumulate
3. The average water velocity when filling the pipeline should not exceed $1 \mathrm{ft} / \mathrm{s}(0.3 \mathrm{~m} / \mathrm{s})$
4. All air should be purged from the pipeline before checking for leaks or performing pressure or acceptance tests on the system
5. If a large quantity of water is needed to increase the pressure during testing, then entrapped air or a leak is possible. Testing should be discontinued until the source of the problem is identified

| Nominal Size |  | Max Filling Rate |  |
| :---: | :---: | :---: | :---: |
| In | mm | gpm | L/s |
| 4 | 100 | 40 | 2.5 |
| 8 | 200 | 157 | 9.9 |
| 10 | 250 | 245 | 15.5 |
| 12 | 300 | 353 | 22.3 |
| 14 | 350 | 480 | 30 |
| 16 | 400 | 627 | 39 |
| 18 | 450 | 793 | 50 |
| 20 | 500 | 979 | 61 |
| 24 | 600 | 1410 | 89 |
| 30 | 750 | 2203 | 139 |
| 36 | 900 | 3173 | 200 |
| 42 | 1050 | 4318 | 272 |
| 48 | 1200 | 5640 | 355 |

## Further References:

Perhaps the most easily accessible work on the subject of air entrapment in pipelines was a film produced in the late 1960's at Colorado State University. It was commissioned by a major pipe manufacturer and clearly shows the effect of air entrapment in pipelines and the importance of properly sizing and situating air release valves. Contact your IPEX technical rep. for a copy on CD.

## Cyclic Fatigue in PVC Pipes

Fatigue is a well known phenomenon that can affect many different materials. Only when a piping system is subjected to extreme cyclic loading conditions does fatigue in PVC pipe become a design factor. Fortunately, there has been a great deal of research done on this topic, and some recent research completed by Dr. A. Moser at Utah State University has contributed greatly to the understanding of this phenomenon.

Dr. Moser has determined that the number of cycles to failure (C) of PVC pipe is a function of the average stress in the pipe walls, as well as the amplitude of the cycles. This builds on previous work done by H.W. Vinson that based the cycles to failure only on the maximum stress in the material.

While cyclic loading is possible in many different applications, it is typically encountered in sewage forcemain and irrigation applications (most water distribution mains or transmission mains have relatively constant pressures). Any
application that has pumps starting up and shutting down at regular intervals (ie more than a couple of times per day) should be analyzed using Dr. Moser's method.

The following graph shows how the average stress and the amplitude are related to the number of cycles to failure

A worked example of a cyclic design for a sewage forcemain can be found in section 3.

## Further Reading:

Vinson, H.W.: "Response of PVC Pipe to Large, Repetitive Pressure Surges" Proceedings of the International Conference on Underground Plastic Pipe (March 1981)

Moser, Folkman, Jeffrey:"Long-Term Cyclic Testing of 6 inch PVC Pipe" Utah State University, (March 2003)

Figure 3 - Resulting Cyclic-Failure Curves for PVC


38

## Thrust Restraint in Gasketed Piping Systems

## Resisting Thrust at Fittings and Valves

At many locations in a pressurized pipeline, an imbalance in hydrostatic forces may occur as a result of the pipeline configuration. These unbalanced forces are called thrust forces. Thrust forces can occur at any point in a piping system where the directional or cross-sectional area of the waterway changes. Pipeline installers must balance these forces by means of thrust blocks or mechanical restraint. Three areas that require restraint are described below.

## - at valves

All valves must be anchored. This includes valves installed in a chamber or in line with the pipe, whether it is operated frequently or only once a year.


Install anchor rods around the valve body or through the mounting lugs and embed the rods in a concrete pour beneath the valve. Valves installed in chambers must also be anchored in this fashion. The critical time for restraint of valves is during opening or closing.

## - at changes in direction (Vertical or Horizontal)

Fittings such as elbows, tees, or dead ends, must be restrained since they involve a significant directional change for the fluid.

## - at reductions in size

The thrust component at reductions in size will depend on the amount of the reduction, and must be adequately restrained.

At each point in the line where thrust forces will develop, pour a concrete block between the fitting and undisturbed native soil at the side of the trench. Use plywood sheets to form the block and control the pour so that the area of contact with the undisturbed trench will provide the necessary support.

## Bearing Strength of Undisturbed Soils

Organic Material (such as Peat, etc.) . . . . . . $0 \mathrm{lb} / \mathrm{ft}^{2}$
Soft Clay . . . . . . . . . . . . . . . . . . . . . . . . $500 \mathrm{lb} / \mathrm{ft}^{2}$
Sand . . . . . . . . . . . . . . . . . . . . . . . . . . $1000 \mathrm{lb} / \mathrm{ft}^{2}$
Sand and Gravel . . . . . . . . . . . . . . . . . . $1500 \mathrm{lb} / \mathrm{ft}^{2}$
Sand \& Gravel with Clay . . . . . . . . . . . . $2000 \mathrm{lb} / \mathrm{ft}^{2}$
Sand \& Gravel Cemented with Clay . . . . . $4000 \mathrm{lb} / \mathrm{ft}^{2}$
Hard Pan . . . . . . . . . . . . . . . . . . . . . . . 5000 lb/ft²
These soil bearing capacities are approximate and conservative. For greater design precision IPEX recommends that soil bearing tests be carried out by a competent soils engineer.

The recommended bearing area to be established by the concrete pour may be given by the engineer. The area ( $\mathrm{ft} .{ }^{2}$ ) may also be calculated by determining the total thrust generated at the fitting. Simply divide the bearing strength of the soil into the thrust developed (Ibs force), as found in the accompanying table. The result is the area of the soil required to resist the thrust (A). The area calculated will be for the area of concrete up against the trench wall (i.e. the back side of the block).


Table 7 - Thrust Developed per 100 psi Pressure (Ibs. force)

| Pipe <br> Diameter <br> in |  | Valves \& Dend <br> Ends, Tees | $90^{\circ}$ <br> Bends | $45^{\circ}$ <br> Bends | $22^{1 / 2^{\circ}}$ <br> Bends | $111 / 4^{\circ}$ <br> Bends |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 | 100 | 1810 | 2560 | 1390 | 635 | 320 |
| 6 | 150 | 3740 | 5290 | 2860 | 1370 | 690 |
| 8 | 200 | 6430 | 9100 | 4920 | 2320 | 1170 |
| 10 | 250 | 9680 | 13680 | 7410 | 3610 | 1820 |
| 12 | 300 | 13690 | 19350 | 10470 | 5080 | 2550 |
| 14 | 350 | 18380 | 25990 | 14100 | 6100 | 3080 |
| 16 | 400 | 23780 | 33630 | 18280 | 7960 | 4020 |
| 18 | 450 | 29860 | 42230 | 22970 | 10060 | 5080 |
| 20 | 500 | 36640 | 51820 | 28180 | 12440 | 6280 |
| 24 | 600 | 52280 | 73930 | 40200 | 17940 | 9060 |
| 30 | 750 | 80425 | 113737 | 61557 | 31500 | 15800 |
| 36 | 900 | 115200 | 162929 | 88181 | 45000 | 22600 |
| 42 | 1050 | 155500 | 219950 | 119000 | 60700 | 30500 |
| 48 | 1200 | 202700 | 286700 | 155200 | 79000 | 39800 |

Note: Pre-cast thrust blocks should not be placed directly against PVC fittings.

## Resisting Thrust in Very Poor Soils

Where the pipeline passes through soils having little or no bearing strength, thrust forces may be restrained by the encasement of the fitting in concrete and the extension of this pour to form a monolith having sufficient inertia to resist the thrusts. It may also be possible to loop tie rods around the fitting and anchor the tie rods into an upstream concrete pour across the trench in more stable soils. Mechanical thrust restraints may also be used in these cases.


Typical thrust block locations. Trim the trench bearing area using hand tools to be sure of undisturbed soil.


This type of hydrant foundation acts as a thrust-block, as an anchorage against frost heave and eliminates washouts from waste-water drain.

## Resisting Vertical Thrust

Where the pipeline will change direction downwards to pass under a creek bed or roadway, etc., upward thrust will be developed at the fitting. Anchor the fitting as though it were a valve, and ensure that the concrete base is keyed into undisturbed soil.


Straps should be 2 inches ( 50 mm ) wide or greater.

## Holding Pipe to Steep Slopes

Normal bedding practices for pipelines installed up a hill will be sufficient to prevent backsliding and decoupling. When the height of cover is less than 6 feet ( 1.8 m ), and the soil conditions are marginal, and where the slope is greater than $20^{\circ}$ ( $36 \%$ slope), a special anchoring method may be desirable. One recommended procedure is to lay the pipe with the bells facing uphill and pour a concrete block behind the bells and keyed into the undisturbed trench sidewalls. Usually every third length of pipe will need to be anchored in this fashion to achieve a stable condition. The use of solvent welded joints for short sections of the pipeline may also be considered on steep slopes.

## Mechanical Thrust Restraints

Several mechanical thrust restraint devices are available which clamp to the wall of the pipe and tie back to a mating collar on the fitting or the pipe bell. The use of these devices may provide the entire thrust restraint necessary at the fitting, in sizes up to 48 inches ( 1200 mm ). The use of several thrust restraints to tie together two or three lengths of pipe on either side of the fitting may be desirable to enlist the clamping effect of the backfill around the pipe barrel. IPEX recommends that the thrust restraint device conforms to the requirements of ASTM F1674-96.
When a thrust restraint device is used the maximum pressure in the pipeline (usually the test pressure) must not exceed the pressure rating of the device.

## Assembly, Installation and testing of PVC Pressure Pipe Systems

Detailed information on how to install IPEX pressure pipes and fittings can be found in IPEX's Installation Guide for PVC Pressure Pipe and Fittings. This guide contains complete information on:

- Receiving and handling pipe shipments
- Trench Preparation
- Lowering Pipe into the trench
- Assembling joints
- Curvature of the pipeline, and assembling to valves and appurtenances
- Machining and chamfering the pipe
- Tapping, flanges and sleeves
- Outside diameter considerations
- Backfilling and installing bedding
- Pressure testing the pipeline
- Installing the pipeline through a casing
- Lubricant usage tables.

The Guide is available from your IPEX rep. or visit our technical library at www.ipexinc.com.


## Section 3 - Design Examples

## Hydraulic and Cyclic Design Example

## Sewage Forcemain Design Example (SI Version)

Select the appropriate pipe size and pressure rating for a sewage forcemain with the following characteristics:
Peak Flow $=450 \mathrm{~L} / \mathrm{s}(7130 \mathrm{GPM})$ Elevation Change (static head): 30 meters (100 feet)
Length: 3000 meters ( 9850 feet)
Average pump cycles per day: 36
System peak pressure during controlled pump operations: $480 \mathrm{kPa}(70 \mathrm{psi})$
Minimum pressure during controlled pump operations: 207 kPa ( 30 psi )
Minimum design life - 50 years

## Step 1 - Select an initial nominal pipe size and pressure rating

A maximum velocity of $1.5 \mathrm{~m} / \mathrm{s}$ ( $5 \mathrm{ft} / \mathrm{s}$ ) is typical in forcemain design. This velocity ensures self cleansing of the line.

$$
\mathrm{Q}=\mathrm{vA} \therefore \mathrm{~A}=\frac{\mathrm{Q}}{\mathrm{v}}
$$

Where,

$$
\begin{aligned}
A & =\text { required pipe cross sectional area, } \mathrm{m}^{2} \\
V & =\text { fluid velocity, } \mathrm{m} / \mathrm{s} \\
Q & =\text { Flow, } \mathrm{m}^{3} / \mathrm{s} \\
A & =\frac{0.450 \mathrm{~m}^{3} / \mathrm{s}}{1.5 \mathrm{~m} / \mathrm{s}}=0.3 \mathrm{~m}^{2}
\end{aligned}
$$

Required diameter:

$$
a=\frac{\pi D^{2}}{4} \therefore D=\sqrt{\frac{4 \mathrm{a}}{\pi}}=\sqrt{\frac{4(0.3)}{\pi}}=0.618 \mathrm{~m}=618 \mathrm{~mm} \text { is the required diameter }
$$

Static pressure is 298 kPa (43 psi), therefore select $600 \mathrm{~mm}\left(24{ }^{\prime \prime}\right)$ nominal diameter SDR51 (long term pressure rating 80 psi ) for initial calculations.
600 mm SDR51 Inside Diameter $=630 \mathrm{~mm}$ (24.8").
Note: The purpose of these initial calculations is to select a nominal pipe size and pressure rating, so the required diameter numbers do not have to match. It is more important to select the proper pipe that corresponds with the initial system static head. This will give a basis for further calculations of dynamic head and surge pressures in the next steps

Step 2 - Calculate dynamic head (friction and minor losses) and total system head
In this step the Hazen-Williams equation is used to calculate the friction losses in the system. For this example we will neglect the minor losses through fittings and valves. For systems with large numbers of fittings, the minor losses should be calculated as they can be significant. Note that the appropriate "C" factor for PVC pipe is 150.
Hazen-Williams Equation:

$$
\mathrm{h}_{\mathrm{f}}=10.654\left(\frac{\mathrm{Q}}{\mathrm{C}}\right)^{\frac{1}{0.54}}\left(\frac{1}{\mathrm{D}^{4.87}}\right) \mathrm{L}=10.654\left(\frac{0.450 \mathrm{~m}^{3} / \mathrm{s}}{150}\right)^{\frac{1}{0.54}}\left(\frac{1}{(0.630 \mathrm{~m})^{4.87}}\right) 3000 \mathrm{~m}=6.4 \mathrm{~m}
$$

The headloss due to friction is 6.4 meters of head or $63 \mathrm{kPa}(9 \mathrm{psi})$. This friction head is added to the static head to get the total system head Note: When using the Hazen-Williams equation with imperial units use the proper imperial form of the equation shown in section 2.
$\mathrm{h}_{\text {sys }}=30 \mathrm{~m}+6.4 \mathrm{~m}=36.4 \mathrm{~m}$ or $357 \mathrm{kPa}(52 \mathrm{psi})$
Therefore, SDR51 with a long term rating (LTR) of 80 psi is adequate for the working pressure requirements of this system.

## Step 3 - Calculate the short term (surge) requirements of the system

In section 2 a method to calculate the surge pressure for a given velocity change in a PVC pipe system was shown. The results of those calculations will be used here without reproducing the actual calculations again. To see exactly how these numbers were arrived at, refer to "Calculating Surge Pressures" in Section 2.

First calculate the actual maximum velocity of a $450 \mathrm{~L} / \mathrm{s}$ flow in 600 mm SDR51:

$$
\mathrm{Q}=\mathrm{va} \therefore \frac{\mathrm{Q}}{\mathrm{a}}=\frac{.450 \mathrm{~m}^{3} / \mathrm{s}}{\left(\frac{\pi(0.630 \mathrm{~m})^{2}}{4}\right)}=1.44 \mathrm{~m} / \mathrm{s}
$$

For every $0.3 \mathrm{~m} / \mathrm{s}$ change in velocity, the surge pressure generated in SDR51 is $75 \mathrm{kPa}(10.8 \mathrm{psi})$.

$$
P_{\mathrm{s}}=\left(\frac{1.44 \mathrm{~m} / \mathrm{s}}{0.3}\right) 75 \mathrm{kPa}=360 \mathrm{kPa}(52 \mathrm{psi})
$$

From Section 2 - the short term rating (STR) of SDR51 is 690 kPa (100psi)
Short term requirements of the system: $357 \mathrm{kPa}+360 \mathrm{kPa}=717 \mathrm{kPa}(104 \mathrm{psi})$
In this case SDR51 is slightly under designed for the short term rating, so we re-iterate the design using SDR41 with an STR of 130 psi. Since the I.D. is slightly different, and the surge generated slightly higher - we re-calculate steps 1 to 3 to obtain the following results:

$$
\begin{aligned}
\mathrm{h}_{\text {sys }} & =30 \mathrm{~m}+6.8 \mathrm{~m}=36.8 \mathrm{~m} \text { or } 358 \mathrm{kPa}(52 \mathrm{psi}) \\
\mathrm{P}_{\mathrm{s}} & =\left(\frac{1.48 \mathrm{~m} / \mathrm{s}}{0.3}\right) 79=389 \mathrm{kPa}(57 \mathrm{psi})
\end{aligned}
$$

Short term requirements of the system: $358 \mathrm{kPa}+389 \mathrm{kPa}=747 \mathrm{kPa}(108 \mathrm{psi})$
STR of SDR41 = 130 psi $(>108 \mathrm{psi})$ therefore adequate for long-term and short-term requirements

## Step 4 - Cyclic Analysis

Recent research by Dr. A. Moser at Utah State University with respect to cyclic fatigue in PVC pipes has both simplified and improved the accuracy of cyclic calculations. Note that the pressures used for the cyclic analysis are those that will occur during controlled start-up and shut down operations. The majority of today's pumping systems are equipped with soft start/stop capabilities, thus minimizing system shocks. The short-term system peak pressure (in this case 108 psi) is often not appropriate for cyclic analysis as it is the peak pressure that would be attained only during uncontrolled events (ie: a power outage), and is not cyclic in nature.

It was given that there are 36 cycles a day which means 36 startups and 36 shut downs for a total of 72 surge events per day.
Controlled max system pressure: $480 \mathrm{kPa}(70 \mathrm{psi})$ \{given
Controlled minimum pressure: $207 \mathrm{kPa}(30 \mathrm{psi})$ \{given
Calculate the average system stress:
$\sigma_{\text {avg }}=\frac{\left(\mathrm{P}_{\text {max }}+\mathrm{P}_{\text {min }}\right)(\mathrm{DR}-1)}{4}=\frac{(480 \mathrm{kPa}+207 \mathrm{kPa})(41-1)}{4}=6879 \mathrm{kPa}(997 \mathrm{psi})$
Calculate the stress amplitude:
$\sigma_{\mathrm{amp}}=\frac{\left(\mathrm{P}_{\max }-\mathrm{P}_{\min }\right)(\mathrm{DR}-1)}{4}=\frac{(480 \mathrm{kPa}-207 \mathrm{kPa})(41-1)}{4}=2730 \mathrm{kPa}(396 \mathrm{psi})$

Figure 3 - Resulting Cyclic-Failure Curves for PVC


Determine the predicted number of cycles to failure using Moser's plot:
From the plot, the predicted cycles to failure are roughly $9 \times 10^{6}$ pump starts and stops.
Calculate cyclic life:
72 events per day $\times 365=26,280$ events per year
$9 \times 10^{6} / 26280=342$ years
Therefore SDR41 is more than adequate for the application

## Transmission Pipe Design Example (Taken from Awwa m23 - PVC Pipe Design \& Installation Manual)

This analysis of a relatively simple pipeline will illustrate the use of the design principles discussed in this guide section. PVC pipe standards offer a variety of pipe strengths and sizes. Ideally, the designer will make selections that minimize capital and operating costs while maintaining an adequate design safety factor.
The project is a 20,000' long PVC water transmission main designed for an ultimate capacity of 4,000 gpm ( 5.76 mgd ).
The profile of the pipeline is shown below. Water is being pumped to a ground storage tank (point f) with a maximum water level of 35 ' from the floor. The centerline of the discharge end of the main, at the tie-in to the storage tank, will be 5' below the tank floor.
Key stations and their elevations along the pipeline are:

| Point | Station | Elevation at Pipe Centerline (ft) |
| :---: | :---: | :---: |
| a | $0+00$ | 600 |
| b | $45+00$ | 670 |
| c | $75+00$ | 720 |
| d | $115+00$ | 800 |
| f | $165+00$ | 940 |

Figure 4 - Pipeline Profile


The objective of the design process will be to select proper DRs of PVC for appropriate sections of pipeline while never exceeding the PR nor the WPR of the pipe at any point. An effort will be made to select DRs that meet the design criteria while providing optimum economic value for the utility or owner.
The key determinant of PVC pressure pipe design is the internal pressure. The pipe dimensions can be found in the AWWA pipe standards. For this example, AWWA Standard C905, Polyvinyl Chloride (PVC) Pressure Pipe and Fabricated Fittings, 14 In . Through 48 In . (350mm through 1,200mm), for Water Transmission and Distribution, was used. The exact pipe dimensions are required to determine the flow velocity. The total pressure in the pipeline at any point is the sum of the static head, the friction loss, and the pressure rise as a result of sudden velocity changes. For simplicity, the selection of PVC pipe in this example will be limited to four PRs in CIOD only (PR 235, 165, 125 and 100).

## Step 1 - Determine the maximum flow velocity

Assume that 20" PVC pipe will be used. In AWWA C905, the heaviest wall shown to be available in 20 " pipe is DR 18. The assumption of beginning with the heaviest wall (i.e., the lowest DR) is recommended for most designs in the initial stage. The first assumption may be confirmed or revised as the design is developed.

Average $I D=$ Average $\mathrm{OD}-2$ (minimum wall thickness $\times 1.06$ )
Note: The tolerance on wall thickness is approximately $+12 \%$. There is no minus tolerance. Manufacturers will generally aim to produce PVC pressure pipe with wall thicknesses about $6 \%$ over minimum.

Assume: 20" DR 18 per AWWA C905

$$
\begin{aligned}
\text { Avg. } I D & =21.60-2(1.200 \times 1.06) \\
& =19.05 \mathrm{in}=1.59 \mathrm{ft} \\
V & =\mathrm{Q} / \mathrm{A}
\end{aligned}
$$

Where,

$$
\begin{aligned}
Q & =\text { Flow in } \mathrm{ft}^{3} / \mathrm{sec}=4,000 \mathrm{gpm} \text { or } 8.91 \mathrm{ft}^{3} / \mathrm{sec} \\
A & =\text { area }, \mathrm{ft}^{2} \\
V & =\text { velocity }, \mathrm{ft} / \mathrm{sec} \\
A & =(3.14)(1.59 / 2)^{2}=1.98 \mathrm{ft}^{2}
\end{aligned}
$$

Therefore,

$$
V=8.91 / 1.98=4.5 \mathrm{ft} / \mathrm{sec}
$$

Because the velocity is within an acceptable range, the design may proceed with 20 " pipe.

## Step 2 - Determine the surge factor

In a transmission pipeline, the amplitude and location of the surge pressure envelope will often be analyzed by computer. For this example, the assumption has been made that the maximum surge pressure will be equal to an instantaneous stop-page of flow at full velocity. In practice, the costs of pipe materials may be significantly reduced through the use of appropriate surge control devices and proper pipeline operating procedures.

The pressure rise resulting from a $V=4.5 \mathrm{ft} / \mathrm{sec}$ instantaneous velocity change in PVC pressure pipes can be charted as follows:

| Dimension Ratio, DR | $\mathbf{1 ~ f t / s e c}$ Surge, $\mathbf{P}_{\mathbf{s}}{ }^{\prime}(\mathbf{p s i})$ | $\mathbf{V} \mathbf{x} \mathbf{P}_{\mathbf{s}}{ }^{\prime}(\mathbf{p s i})$ |
| :---: | :---: | :---: |
| 41 | 11.4 | 51.3 |
| 32.5 | 12.8 | 57.6 |
| 25 | 14.7 | 66.2 |
| 18 | 17.4 | 78.3 |

## Step 3 - Determine the WPR for each of the DRs of Step 2

The WPR is a job-specific pressure rating of the pipe, taking into account the maximum possible surges versus the short-term strength of the pipe. The WPR may be either higher or lower than the PR of the pipe, depending on the flow conditions. The lower value between the WPR and the PR should be used as the upper limit for system steady-state operating pressure.
$W P R=\mathrm{STR}-\mathrm{V} \times \mathrm{P}_{\mathrm{s}}{ }^{\prime}$

| DR | $\mathbf{S T R}(\mathbf{p s i})$ | $\mathbf{V x P}_{\mathbf{s}}{ }^{\prime}(\mathbf{p s i})$ | WPR (psi) | PR (psi) |
| :---: | :---: | :---: | :---: | :---: |
| 41 | 130 | 51.3 | 78.7 | 100 |
| 32.5 | 165 | 57.6 | 107.4 | 125 |
| 25 | 215 | 66.2 | 148.8 | 165 |
| 18 | 300 | 78.3 | 221.7 | 235 |

It can be seen that the governing parameter for the pressure design of this example will be the WPR analysis since it is lower than the PR of each DR.

## Step 4 - Determine the friction loss $f$ under full-flow conditions

Continue to assume DR 18 for this calculation because this pipe will produce slightly greater losses than the other DRs under consideration. The result will be conservative for all design operations.

The Hazen-Williams equation is convenient to use:

$$
f=0.2083(100 / \mathrm{C})^{1.852} \frac{\mathrm{Q}^{1.852}}{\mathrm{~d}_{\mathrm{i}}^{4.8655}}
$$

Where,
$f=$ friction head, ft of water per 100 ft of pipe
$d_{i}=$ inside diameter of pipe, in.
$Q=$ flow, gpm
$C=$ flow coefficient, 150 for PVC
Substituting for 20 " PR 235 pipe, where $\boldsymbol{d}=19.05$ in
$f=0.273 \mathrm{ft}$ of water per 100 ft of pipeline
$=0.118 \mathrm{psi}$ per 100 ft (station) of pipeline

## Step 5 - Determine the pressures at key points in the pipeline under steady-state, full-flow conditions

This pressure, P , at any point is the sum of the static head as a result of difference in elevations and the friction loss.
Referring to Figure 4, the pressure at key points can be calculated as follows:
Starting at the storage tank:

| Station 200 + 00 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Static Head <br> or $40 \mathrm{ft} \times(0.43 \mathrm{psi} / \mathrm{ft})$ | $=$ | 980-940 | $\begin{aligned} & = \\ & = \end{aligned}$ | $\begin{array}{r} 40 \mathrm{ft} \\ 17.3 \mathrm{psi} \end{array}$ |
| Station $165+00$ |  |  |  |  |
| Static Head | = | (980-940) ft x (0.43 psi/ft) | $=$ | 17.3 psi |
| Friction Head | = | $(3,500 \mathrm{ft}) \times(0.118 \mathrm{psi} / 100 \mathrm{ft})$ | = | 4.1 psi |
| Total Head |  |  | = | 21.4 psi |
| Station $115+00$ |  |  |  |  |
| Static Head | $=$ | (980-800) ft x (0.43 psi/ft) | $=$ | 77.4 psi |
| Friction Head | = | $(8,500 \mathrm{ft}) \times(0.118 \mathrm{psi} / 100 \mathrm{ft})$ | = | 10.0 psi |
| Total Head |  |  | = | 87.4 psi |
| Station $75+00$ |  |  |  |  |
| Static Head | $=$ | (980-720) ft x (0.43 psi/ft) | = | 111.8 psi |
| Friction Head | $=$ | $(12,500 \mathrm{ft}) \times(0.118 \mathrm{psi} / 100 \mathrm{ft})$ | = | 14.8 psi |
| Total Head |  |  | = | 126.6 psi |
| Station $45+00$ |  |  |  |  |
| Static Head | = | (980-670) ft x (0.43 psi/ft) | = | 133.3 psi |
| Friction Head | $=$ | $(15,500 \mathrm{ft}) \times(0.118 \mathrm{psi} / 100 \mathrm{ft})$ | = | 18.3 psi |
| Total Head |  |  | = | 151.6 psi |
| Station $0+00$ |  |  |  |  |
| Static Head | $=$ | (980-600) ft x (0.43 psi/ft) | $=$ | 163.4 psi |
| Friction Head | = | $(20,000 \mathrm{ft}) \times(0.118 \mathrm{psi} / 100 \mathrm{ft})$ | $=$ | 23.6 psi |
| Total Head |  |  | $=$ | 187.0 psi |

The pressure, P , at each of the key points are summarized as follows:

| Point | Station | Static Head (psi) | Friction Head (psi) | Pressure, P (psi) |
| :---: | :---: | :---: | :---: | :---: |
| f | $200+00$ | 17.3 | 0 | 17.3 |
| e | $165+00$ | 17.3 | 4.1 | 21.4 |
| d | $115+00$ | 77.4 | 10.0 | 87.4 |
| c | $75+00$ | 111.8 | 14.8 | 126.6 |
| b | $45+00$ | 133.3 | 18.3 | 151.6 |
| a | $0+00$ | 163.4 | 23.6 | 187.0 |

## Step 6 - Determine the appropriate DR of pipe for each section of the pipeline

From previous calculations in Step 3, DR 18 PVC pressure pipe has a working pressure rating 221.7 psi. For the next greater DR, DR 25, the WPR is 148.8 psi. Therefore, DR 18 is selected to start out at the pumphouse until a point in the system where the operating pressure, P, drops to be equal to the WPR of DR 25 . At this point, DR 25 may be used. Subsequent steps will determine the starting points for DR 32.5 as well as DR 41.

It can be seen from the above summary of pressures by section that the transition to DR 25 will occur between Stations $45+00$ and $75+00$, in section bc. To pinpoint the exact location, the pressure gradient for that section must be calculated.

$$
\begin{aligned}
\Delta P(b c) & =\frac{(\mathrm{Pc}+\mathrm{Pb})}{\text { Station Length of } \mathrm{bc}} \\
& =\frac{126.6 \mathrm{psi}-151.6 \mathrm{psi}}{(75-45) \times(100 \mathrm{ft})} \\
& =-0.83 \mathrm{psi} / 100 \mathrm{ft}
\end{aligned}
$$

The length beyond Station $45+00$ (point b) can be calculated as follows:

```
Station Length \(=\frac{\mathrm{WPR}(\mathrm{DR} 25)-\mathrm{Pb}}{\Delta \mathrm{P}(\mathrm{bc})}\)
    \(=\frac{(148.8 \mathrm{psi})-(151.6 \mathrm{psi})}{-0.83 \mathrm{psi} / 100 \mathrm{ft}}\)
    \(=337 \mathrm{ft}\) (i.e., at 337 ft downstream of Station \(45+00\) )
```

Therefore, begin using DR 25 at Station $48+37$.
Similarly, the transition point for DR 32.5 can be found.
From the summary of pressures and knowing the WPR of DR 32.5 is 107.4 psi, DR 32.5 can be used between Station $75+00$ and Station $115+00$, i.e., section cd.

First, calculate the pressure gradient in section cd.

$$
\begin{aligned}
\Delta P(c d) & =\frac{(\mathrm{Pd}-\mathrm{Pc})}{\text { Station Length of cd }} \\
& =\frac{87.4 \mathrm{psi}-126.6 \mathrm{psi}}{(115-75) \times(100 \mathrm{ft})} \\
& =-0.98 \mathrm{psi} / 100 \mathrm{ft}
\end{aligned}
$$

Next, the Station Length beyond Station $75+00$ can be calculated:

```
Station Length \(=\frac{\text { WPR(DR 32.5) }-\mathrm{Pc}}{\Delta \mathrm{P}(\mathrm{cd})}\)
    \(=\frac{(107.4 \mathrm{psi})-(126.6 \mathrm{psi})}{-0.98 \mathrm{psi} / 100 \mathrm{ft}}\)
    \(=1,959 \mathrm{ft}\) (i.e., at \(1,959 \mathrm{ft}\) downstream of Station \(75+00\) )
```

Therefore, begin using DR 32.5 at Station $94+59$.

Similarly, it can be calculated where DR 41 usage may begin.
From review of the summary of pressures and knowing the WPR of DR 41 is 78.7 psi, the range for DR 41 begins between Station $115+00$ and Station $165+00$, i.e., section de.
First, calculate the pressure gradient in section de.

$$
\begin{aligned}
\Delta P(d e) & =\frac{(\mathrm{Pe}-\mathrm{Pd})}{\text { Station Length of de }} \\
& =\frac{21.4 \mathrm{psi}-87.4 \mathrm{psi}}{(165-115) \times(100 \mathrm{ft})} \\
& =-1.32 \mathrm{psi} / 100 \mathrm{ft}
\end{aligned}
$$

Next, the Station Length beyond point d:

```
Station Length \(=\frac{\text { WPR(DR 41) }-\mathrm{Pd}}{\Delta \mathrm{P}(\mathrm{de})}\)
    \(=\frac{(78.7 \mathrm{psi})-(87.4 \mathrm{psi})}{-1.32 \mathrm{psi} / 100 \mathrm{ft}}\)
    \(=659 \mathrm{ft}\) (i.e., at 659 ft downstream of Station \(115+00\) )
```

Therefore, DR 41 may begin usage at Station $121+59$ and continue for the duration of the pipeline up to its terminus at the reservoir.

The design for internal pressure may be summarized as follows:

| Distance from Pumphouse (ft) | Use 20 in. | Pressure Gradient (psi) |
| :---: | :---: | :---: |
| $0-4.837$ | DR 18 (PR 235) | $187.0-148.8$ |
| $4,837-9,459$ | DR 25 (PR 165) | $148.8-107.4$ |
| $9,459-12,159$ | DR 32.5 (PR 125) | $107.4-78.7$ |
| $12,159-20,000$ | DR 41 (PR 100) | $78.7-17.3$ |

In this example of a 3.8 mile pipeline, the designer has the opportunity to make significant cost savings through the use of several PVC pipe pressure ratings. Computer modeling may disclose even further potential savings by showing exactly where and how surge control is most effective. (Note that the above pipe selection was made assuming that the potential exists for the instantaneous stoppage of flow.)

If the pipeline is operated in a cycle mode (i.e., like some sewage force mains), an analysis of fatigue life should be made. Both present and future modes of operation should be examined.

## Section Four: Appendices

## Appendix A: References

1 Duranceau, Schiff, Bell. "Electrical Grounding, Pipe Integrity and Shock Hazard", Journal of the AWWA, July 1998, pp. 40-51

2 Hulsmann, Nowack,"70 Years of Experience with PVC Pipes" Conference Paper, Plastic Pipes XII, Milan, April 2004

3 Jenkins, Thompson,"Review of Water Industry Plastic Pipe Practices", AWWA Research Foundation, 1987

4 Berens, A.R., "Prediction of Chemical Permeation through PVC Pipe", Journal of the AWWA, November 1985

5 Hoogensen Metallurgical Engineering Ltd.," Examination of Submitted PVC Pipe Section", Report to IPEX, December 1998

6 Uni-Bell PVC Pipe Association, "Handbook of PVC Pipe - Design and Construction", fourth edition, (August 2001)

## Appendix B: Reference Tables and Conversion Charts

Table B-1 Pipe Capacity
Table B-2 Weights of Water
Table B-3 Decimal \& Millimeter Equivalents of Fractions
Table B-4 Volume Conversion
Table B-5 Pressure Conversion
Table B-6 Flow Conversion
Table B-7 Temperature Conversion
Table B-8 Length Conversion

## Appendix C: Useful Formulas

- Area of a Circle
- Circumference of a Circle
- Length of Circular Arc
- Area of Circle Sector
- Equation of a Circle (cartesian coordinates)
- Equation of a Line (quadratic formula)
- Basic Trigonometric Functions
- Area of an Ellipse
- Circumference of an Ellipse
- Area of a Triangle
- Area of a Trapezoid
- Area of a Parallelogram
- Surface Area of a Sphere
- Volume of a Sphere
- Surface Area of a Cylinder
- Volume of a Cylinder
- Surface Area of an Elliptical Tank
- Volume of an Elliptical Tank
- Surface Area of a Cone
- Volume of a Cone
- Surface Area of a Rectangular Solid
- Volume of a Rectangular Solid


## Table B-1 Pipe Capacity

| Pipe Size <br> (in.) | Outside Diameter - IPS OD Pipe |  |  | Volume for $\mathbf{1}$ foot length of pipe |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | inch | feet | $\mathbf{c m}$ | $\mathbf{i n}^{\mathbf{3}}$ | $\mathbf{f t}^{\mathbf{3}}$ | $\mathbf{c m}^{\mathbf{3}}$ | US Gal | Imp Gal |
| $1 / 4$ | 0.250 | 0.021 | 0.098 | 0.589 | 0.0003 | 9.648 | 0.003 | 0.002 |
| $3 / 8$ | 0.375 | 0.031 | 0.148 | 1.325 | 0.001 | 21.708 | 0.006 | 0.005 |
| $1 / 2$ | 0.500 | 0.042 | 0.197 | 2.355 | 0.001 | 38.591 | 0.010 | 0.008 |
| $3 / 4$ | 0.750 | 0.063 | 0.295 | 5.299 | 0.003 | 86.831 | 0.023 | 0.019 |
| 1 | 1.000 | 0.083 | 0.394 | 9.420 | 0.005 | 154.366 | 0.041 | 0.034 |
| $1-1 / 4$ | 1.250 | 0.104 | 0.492 | 14.719 | 0.009 | 241.196 | 0.064 | 0.053 |
| $1-1 / 2$ | 1.500 | 0.125 | 0.591 | 21.195 | 0.012 | 347.322 | 0.092 | 0.076 |
| 2 | 2.000 | 0.167 | 0.787 | 37.680 | 0.022 | 617.462 | 0.163 | 0.136 |
| 3 | 3.000 | 0.250 | 1.181 | 84.780 | 0.049 | $1,389.290$ | 0.367 | 0.306 |
| 4 | 4.000 | 0.333 | 1.575 | 150.720 | 0.087 | $2,469.849$ | 0.652 | 0.543 |
| 5 | 5.000 | 0.417 | 1.969 | 235.500 | 0.136 | $3,859.139$ | 1.019 | 0.849 |
| 6 | 6.000 | 0.500 | 2.362 | 339.120 | 0.196 | $5,557.159$ | 1.468 | 1.222 |
| 8 | 8.000 | 0.667 | 3.150 | 602.880 | 0.349 | $9,879.395$ | 2.610 | 2.173 |
| 10 | 10.000 | 0.833 | 3.937 | 942.000 | 0.545 | $15,436.554$ | 4.078 | 3.396 |
| 12 | 12.000 | 1.000 | 4.724 | $1,356.480$ | 0.785 | $22,228.638$ | 5.872 | 4.890 |
| 14 | 14.000 | 1.167 | 5.512 | $1,846.320$ | 1.068 | $30,255.646$ | 7.993 | 6.655 |
| 16 | 16.000 | 1.333 | 6.299 | $2,411.520$ | 1.396 | $39,517.578$ | 10.439 | 8.693 |
| 18 | 18.000 | 1.500 | 7.087 | $3,052.080$ | 1.766 | $50,014.435$ | 13.212 | 11.002 |
| 20 | 20.000 | 1.667 | 7.874 | $3,768.000$ | 2.181 | $61,746.216$ | 16.312 | 13.582 |
| 24 | 24.000 | 2.000 | 9.449 | $5,425.920$ | 3.140 | $88,914.551$ | 23.489 | 19.559 |

## Table B-2 Weights of Water

| Units of Volume | Weight |  |
| :--- | :---: | :---: |
|  | pounds | kilograms |
| 1 US Gallon | 8.350 | 3.791 |
| 1 Imperial Gallon | 10.020 | 4.549 |
| 1 litre | 2.210 | 1.003 |
| 1 cubic yard | $1,685.610$ | 765.267 |
| 1 cubic foot | 62.430 | 28.343 |
| 1 cubic inch | 0.036 | 0.016 |
| 1 cubic $c m$ | 0.002 | 0.001 |
| 1 cubic metre | $2,210.000$ | $1,000.000$ |

## Table B-3 Decimal \& Millimeter Equivalents of Fractions

| Inches |  | Millimeters |
| :---: | :---: | :---: |
| Fractions | Decimals |  |
| 1/64 | 0.015625 | 0.397 |
| 1/32 | 0.03125 | 0.794 |
| 3/64 | 0.046875 | 1.191 |
| 1/16 | 0.0625 | 1.588 |
| 5/64 | 0.078125 | 1.984 |
| 3/32 | 0.09375 | 2.381 |
| 7/64 | 0.109375 | 2.778 |
| 1/8 | 0.125 | 3.175 |
| 9/64 | 0.140625 | 3.572 |
| 5/32 | 0.15625 | 3.969 |
| 11/64 | 0.171875 | 4.366 |
| 3/16 | 0.1875 | 4.763 |
| 13/64 | 0.203125 | 5.159 |
| 7/32 | 0.21875 | 5.556 |
| 15/64 | 0.23475 | 5.953 |
| 1/4 | 0.250 | 6.350 |
| 17/64 | 0.265625 | 6.747 |
| 9/32 | 0.28125 | 7.144 |
| 19/64 | 0.296875 | 7.541 |
| 5/16 | 0.3125 | 7.938 |
| 21/64 | 0.328125 | 8.334 |
| 11/32 | 0.34375 | 8.731 |
| 23/64 | 0.359375 | 9.128 |
| 3/8 | 0.375 | 9.525 |
| 25/64 | 0.390625 | 9.922 |
| 13/32 | 0.40625 | 10.319 |
| 27/64 | 0.421875 | 10.716 |
| 7/16 | 0.4375 | 11.113 |
| 29/64 | 0.453125 | 11.509 |
| 15/32 | 0.46875 | 11.906 |
| 31/64 | 0.484375 | 12.303 |
| 1/2 | 0.500 | 12.700 |


| Inches |  | Millimeters |
| :---: | :--- | :---: |
| Fractions | Decimals |  |
| $33 / 64$ | 0.515625 | 13.097 |
| $17 / 32$ | 0.53125 | 13.494 |
| $35 / 64$ | 0.546875 | 13.891 |
| $9 / 16$ | 0.5625 | 14.288 |
| $37 / 64$ | 0.578125 | 14.684 |
| $19 / 32$ | 0.59375 | 15.081 |
| $39 / 64$ | 0.609375 | 15.478 |
| $5 / 8$ | 0.625 | 15.875 |
| $41 / 64$ | 0.640625 | 16.272 |
| $21 / 32$ | 0.65625 | 16.669 |
| $43 / 64$ | 0.671875 | 17.066 |
| $11 / 16$ | 0.6875 | 17.463 |
| $45 / 64$ | 0.703125 | 17.859 |
| $23 / 32$ | 0.71875 | 18.256 |
| $47 / 64$ | 0.734375 | 18.653 |
| $3 / 4$ | 0.750 | 19.050 |
| $49 / 64$ | 0.765625 | 19.447 |
| $25 / 32$ | 0.78125 | 19.844 |
| $51 / 64$ | 0.796875 | 20.241 |
| $13 / 16$ | 0.8125 | 20.638 |
| $53 / 64$ | 0.828125 | 21.034 |
| $27 / 32$ | 0.83475 | 21.431 |
| $55 / 64$ | 0.859375 | 21.828 |
| $7 / 8$ | 0.875 | 22.225 |
| $57 / 64$ | 0.890625 | 22.622 |
| $29 / 32$ | 0.90625 | 23.019 |
| $59 / 64$ | 0.921875 | 23.416 |
| $15 / 16$ | 0.9375 | 23.813 |
| $61 / 64$ | 0.953125 | 24.209 |
| $31 / 32$ | 0.96875 | 24.606 |
| $63 / 64$ | 0.984375 | 25.003 |
| 1 | 1.000 | 25.400 |
|  |  |  |

## Table B-4 Volume Conversion

| Units of Volume | $\mathbf{i n}^{\mathbf{3}}$ | $\mathbf{f t}^{\mathbf{3}}$ | $\mathbf{y d}^{\mathbf{3}}$ | $\mathbf{c m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | liter | U.S. gal. | Imp. gal. |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| cubic inch | 1 | 0.00058 | - | 16.387 | - | 0.0164 | 0.0043 | 0.0036 |
| cubic foot | 1728 | 1 | 0.0370 | $28,317.8$ | 0.0283 | 28.32 | 7.481 | 6.229 |
| cubic yard | 46,656 | 27 | 1 | - | 0.7646 | 764.55 | 201.97 | 168.8 |
| cubic centimeter | 0.0610 | - | - | 1 | - | 0.001 | 0.0003 | 0.0002 |
| cubic meter | $61,023.7$ | 35.31 | 1.308 | - | 1 | 1000 | 264.17 | 220.0 |
| liter | 61.02 | 0.0353 | 0.0013 | 1000 | 0.001 | 1 | 0.2642 | 0.22 |
| U.S. gallon | 231 | 0.1337 | 0.0050 | 3785.4 | 0.0038 | 3.785 | 1 | 0.8327 |
| Imp. gallon | 277.42 | 0.1605 | 0.0059 | 4546.1 | 0.0045 | 4.546 | 1.201 | 1 |

Table B-5 Pressure Conversion

| Units of Pressure | atm | bar | 1b/in ${ }^{2}$ | $11 / 4 / t^{2}$ | $\mathrm{kg} / \mathrm{cm}^{2}$ | $\mathrm{kg} / \mathrm{m}^{2}$ | inch $\mathrm{H}_{2} \mathrm{O}$ | inch Hg | inch air | $\mathrm{ft}_{\mathrm{H}} \mathrm{O}$ | $f t$ air | mm Hg | mm H20 | kilopascal | $\mathrm{N} / \mathrm{m}^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| atmosphere (atm) | 1 | 0.987 | 0.068 | - | 0.968 | - | 0.002 | 0.033 | - | 0.029 | - | 0.001 | - | 0.01 | - |
| bar | 1.013 | 1 | 0.069 | - | 0.981 | - | 0.002 | 0.034 | - | 0.03 | - | 0.001 | - | 0.01 | - |
| pound per square inch (psi) | 14.7 | 14.5 | 1 | 0.007 | 14.22 | 0.001 | 0.036 | 0.491 | - | 0.434 | 0.001 | 0.019 | 0.001 | 0.145 | - |
| pound <br> per square foot (psf) | 2,116 | 2,089 | 144 | 1 | 2,048 | 0.205 | 5.2 | 70.73 | 0.006 | 62.43 | 0.076 | 2.784 | 0.205 | 20.89 | 0.021 |
| kilogram per square centimeter | 1.033 | 1.02 | 0.07 | - | 1 | 0.0001 | 0.003 | 0.035 | - | 0.03 | - | 0.001 | - | 0.01 | - |
| kilogram per square meter | 10,332 | 10,197 | 703 | 4.88 | 10,000 | 1 | 25.4 | 345.3 | 0.031 | 304.8 | 0.373 | 13.6 | 1 | 101.97 | 0.102 |
| inch of water ( $\left.\mathrm{H}_{2} \mathrm{O}\right)\left(4^{\circ} \mathrm{C}\right)$ | 406.78 | 401.46 | 27.68 | 0.192 | 393.7 | 0.039 | 1 | 13.6 | 0.001 | 12 | 0.015 | 0.535 | 0.039 | 4.015 | 0.004 |
| inch of mercury ( Hg ) ( $0^{\circ} \mathrm{C}$ ) | 29.921 | 29.53 | 2.036 | 0.014 | 28.96 | 0.003 | 0.074 | 1 | - | 0.883 | 0.001 | 0.039 | 0.003 | 0.295 | - |
| inch of air ( $15^{\circ} \mathrm{C}$ ) | 332,005 | 327,664 | 22,592 | 148.7 | 321,328 | 32.13 | 816.2 | 11,096 | 1 | 9,794 | 12 | 436.8 | 32.13 | 3,277 | 3.106 |
| foot of water ( $4^{\circ} \mathrm{C}$ ) | 33.9 | 33.46 | 2.307 | 0.016 | 32.81 | 0.003 | 0.083 | 1.133 | - | 1 | - | 0.045 | 0.003 | 0.335 | - |
| foot of air ( $15^{\circ} \mathrm{C}$ ) | 27,677 | 27,305 | 1,883 | 13.07 | 26,777 | 2.678 | 0.006 | 924.7 | 0.083 | 816.2 | 1 | 36.4 | 2.678 | 273.1 | 0.273 |
| millimeter of mercury ( $0^{\circ} \mathrm{C}$ ) | 760 | 750 | 51.71 | 0.36 | 735.6 | 0.074 | 1.868 | 25.4 | 0.002 | 22.42 | 0.027 | 1 | 0.074 | 7.5 | 0.008 |
| mill imeter of water ( $4^{\circ} \mathrm{C}$ ) | 10,332 | 10,197 | 703 | 4.88 | 10,000 | 1 | 25.4 | 345.3 | 0.031 | 304.8 | 0.373 | 13.6 | 1 | 101.97 | 0.102 |
| kilopascal (kP) | 101.3 | 100 | 6.89 | 0.048 | 98.07 | 0.01 | 0.249 | 3.386 | - | 2.99 | 0.004 | 0.133 | 0.01 | 1 | 0.001 |
| Newton per square meter | - | - | - | 0.021 | - | 0.102 | 0.004 | - | 3.277 | - | 0.273 | 0.008 | 0.102 | 0.001 | 1 |

## Table B-6 Flow Conversion

| Units of Flow Rate | US gps | US gpm | US gph | US gpd | Imp gps | Imp gpm | Imp gph | Imp gpd | liters/sec | liters/min | liters/hr | liters/day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| US gal/sec (gps) | 1 | 0.017 | - | - | 1.2 | 0.02 | - |  | 0.264 | 0.004 |  | - |
| US gal/min (gpm) | 60 | 1 | 0.017 | 0.001 | 72.06 | 1.2 | 0.02 | 0.001 | 15.85 | 0.264 | 0.004 | - |
| US gal/hr (gph) | 3,600 | 60 | 1 | 0.042 | 4,323 | 72.06 | 1.2 | 0.05 | 951.02 | 15.85 | 0.264 | 0.011 |
| US gal/day (gpd) | 86,400 | 1,440 | 24 | 1 | 103,762 | 1,729.40 | 28.82 | 1.2 | 22,824 | 380.41 | 6.34 | 0.264 |
| Imperial gal/sec | 0.833 | 0.014 | - | - | 1 | 0.017 | - | - | 0.22 | 0.004 | - | - |
| Imperial gal/min | 49.96 | 0.833 | 0.014 | 0.001 | 60 | 1 | 0.017 | 0.001 | 13.2 | 0.22 | 0.004 | - |
| Imperial gal/hr | 2,997.60 | 49.96 | 0.833 | 0.035 | 3,600 | 60 | 1 | 0.042 | 791.89 | 13.2 | 0.22 | 0.009 |
| Imperial gal/day | 71,943 | 1,199 | 19.98 | 0.833 | 86,400 | 1,440 | 24 | 1 | 19,005 | 316.76 | 5.279 | 0.22 |
| Liters/sec | 3.79 | 0.063 | 0.002 | - | 4.55 | 0.076 | 0.001 | - | 1 | 0.017 | - | - |
| Liters/min | 227.12 | 3.785 | 0.063 | 0.003 | 272.77 | 4.55 | 0.076 | 0.003 | 60 | . | 0.017 | 0.001 |
| Liters/hr | 13,627 | 227.12 | 3.785 | 0.158 | 16,366 | 272.77 | 4.55 | 0.189 | 3,600 | 60 | 1 | 0.042 |
| Liters/day | 327,060 | 5,451 | 90.85 | 3.785 | 392,782 | 6,546 | 109.11 | 4.55 | 86,400 | 1,440 | 24 | 1 |
| Cubic ft/sec (cfs) | 0.134 | 0.002 | - | - | 0.161 | 0.003 | - | - | 0.035 | 0.001 | - | - |
| Cubic $\mathrm{ft} / \mathrm{min}$ (cfm) | 8.02 | 0.134 | 0.002 | - | 9.633 | 0.161 | 0.003 | - | 2.119 | 0.035 | 0.001 | - |
| Cubic ft/hr (cfh) | 481.25 | 8.02 | 0.134 | 0.006 | 577.96 | 9.63 | 0.161 | 0.007 | 127.13 | 2.119 | 0.035 | 0.001 |
| Cubic ft/day (cfd) | 11,550 | 192.5 | 3.21 | 0.134 | 13,871 | 231.18 | 3.853 | 0.161 | 3,051.20 | 50.85 | 0.848 | 0.001 |
| Acre in/min | 0.002 | - | - | - | 0.003 | - | - | - | 0.001 | - | - | - |
| Acre in/hr | 0.133 | 0.002 | - | - | 0.159 | 0.003 | - | - | 0.035 | - | - | - |
| Acre in/day | 3.182 | 0.053 | 0.001 | - | 3.821 | 0.064 | 0.001 | - | 0.841 | 0.001 | - | - |
| Cubic m/sec | 0.004 | - | - | - | 0.005 | - | - | - | 0.001 | - | - | - |
| Cubic m/min | 0.227 | 0.004 | - | - | 0.273 | 0.005 | - | - | 0.06 | 0.001 | - | - |
| Cubic m/hr | 13.628 | 0.227 | 0.004 | - | 16.366 | 0.273 | 0.005 | - | 3.6 | 0.06 | 0.001 | - |
| Cubic m/day | 327.06 | 5.451 | 0.091 | 0.004 | 392.78 | 6.546 | 0.109 | 0.005 | 86.4 | 1.44 | 0.024 | 0.001 |


| Units of Flow Rate | $\mathrm{ft}^{3} / \mathrm{sec}$ | $\mathrm{ft}^{3} / \mathrm{min}$ | $\mathrm{ft}^{3} / \mathrm{hr}$ | ft/3ay | Acre in/min | Acre in/hr | Acre in/day | $\mathrm{m}^{3} / \mathrm{sec}$ | $\mathrm{m}^{3} / \mathrm{min}$ | $\mathrm{m}^{3} / \mathrm{hr}$ | m³/day |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| US gal/sec (gps) | 7.48 | 0.125 | 0.002 | - | 452.6 | 7.54 | 0.31 | 264.2 | 4.4 | 0.073 | 0.003 |
| US gal/min (gpm) | 448.8 | 7.48 | 0.125 | 0.005 | 27,154 | 452.6 | 18.86 | 15,850 | 264.2 | 4.403 | 0.183 |
| US gal/hr (gph) | 26,930 | 448.83 | 7.481 | 0.312 | $1.629 \mathrm{E}+06$ | 27,154 | 1,131 | 951,019 | 15,850 | 264.17 | 11.007 |
| US gal/day (gpd) | 646,317 | 10,772 | 179.53 | 7.481 | $3.910 \mathrm{E}+07$ | 651,703 | 27,154 | $2.282 \mathrm{E}+07$ | 380,408 | 6,340 | 264.17 |
| Imperial gal/sec | 6.229 | 0.104 | 0.002 | - | 376.8 | 6.28 | 0.26 | 220 | 3.67 | 0.061 | 0.003 |
| Imperial gal/min | 373.73 | 6.229 | 0.104 | 0.004 | 22,611 | 376.8 | 15.7 | 13,198 | 220 | 3.666 | 0.153 |
| Imperial gal/hr | 22,424 | 373.73 | 6.229 | 0.259 | $1.357 \mathrm{E}+06$ | 22,611 | 942.1 | 791,889 | 13,198 | 220 | 9.165 |
| Imperial gal/day | 538,171 | 8,970 | 149.49 | 6.229 | $3.256 \mathrm{E}+07$ | 542,656 | 22,611 | $1.901 \mathrm{E}+07$ | 316,756 | 5,279 | 220 |
| Liters/sec | 28.32 | 0.472 | 0.008 | - | 1,713 | 28.6 | 1.19 | 1,000 | 16.67 | 0.278 | 0.012 |
| Liters/min | 1,699 | 28.32 | 0.472 | 0.2 | 102,790 | 1,713 | 71.38 | 60,000 | 1,000 | 16.67 | 0.694 |
| Liters/hr | 101,941 | 1,669 | 28.32 | 1.18 | $6.167 \mathrm{E}+06$ | 102,790 | 4,283 | $3.600 \mathrm{E}+06$ | 60,000 | 1,000 | 42.67 |
| Liters/day | 2,446,575 | 40,776 | 679.6 | 28.32 | 1.480E+08 | $2.467 \mathrm{E}+06$ | 102,790 | 8.640E+07 | $1.440 \mathrm{E}+06$ | 24,000 | 1,000 |
| Cubic ft/sec (cfs) | 1 | 0.017 | - | - | 60.5 | 1.008 | 0.042 | 35.31 | 0.589 | 0.01 | - |
| Cubic ft/min (cfm) | 60 | 1 | 0.017 | - | 3,630 | 60.5 | 2.52 | 2,119 | 35.31 | 0.59 | 0.025 |
| Cubic ft/hr (cfh) | 3,600 | 60 | 1 | 0.042 | 217,800 | 3,630 | 151.25 | 127,133 | 2,119 | 35.31 | 1.471 |
| Cubic ft/day (cfd) | 86,400 | 1,440 | 24 | 1 | 5.227E+06 | 87,120 | 3,630 | 3,051,187 | 50,853 | 847.55 | 35.31 |
| Acre in/min | 0.017 | - | - | - | 1 | 0.017 | 0.001 | 0.584 | 0.01 | - | - |
| Acre in/hr | 0.992 | 0.001 | - | - | 60 | 1 | 0.042 | 35.02 | 0.584 | 0.01 | - |
| Acre in/day | 23.8 | 0.033 | 0.006 | - | 1,440 | 24 | 1 | 840.55 | 14.001 | 0.233 | 0.001 |
| Cubic m/sec | 0.028 | - | - | - | 1.71 | 0.029 | 0.001 | 1 | 0.017 | - | - |
| Cubic m/min | 1.7 | 0.028 | - | - | 102.8 | 1.71 | 0.071 | 60 | 1 | 0.017 | 0.001 |
| Cubic m/hr | 101.94 | 1.7 | 0.028 | 0.001 | 6,167 | 102.8 | 4.283 | 3,600 | 60 | 1 | 0.042 |
| Cubic m/day | 2446.6 | 40.78 | 0.68 | 0.028 | 148,018 | 2,467 | 102.79 | 86,400 | 1,400 | 24 | 1 |

58

## Table B-7 Temperature Conversion

| ${ }^{\text {o }}$ F | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\text {a }}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -60 | -51 | 22 | -5.6 | 50 | 10.0 | 78 | 25.6 | 160 | 71 |
| -50 | -46 | 23 | -5.0 | 51 | 10.6 | 79 | 26.1 | 170 | 77 |
| -40 | -40 | 24 | -4.4 | 52 | 11.1 | 80 | 26.7 | 180 | 82 |
| -30 | -34 | 25 | -3.9 | 53 | 11.7 | 81 | 27.2 | 190 | 88 |
| -20 | -29 | 26 | -3.3 | 54 | 12.2 | 82 | 27.8 | 200 | 92 |
| -10 | -23.0 | 27 | -2.8 | 55 | 12.8 | 83 | 28.3 | 210 | 99 |
| 0 | -17.8 | 28 | -2.2 | 56 | 13.3 | 84 | 28.9 | 212 | 100 |
| 1 | -17.2 | 29 | -1.7 | 57 | 13.9 | 85 | 29.4 | 220 | 104 |
| 2 | -16.7 | 30 | -1.1 | 58 | 14.4 | 86 | 30.0 | 230 | 110 |
| 3 | -16.1 | 31 | -0.6 | 59 | 15.0 | 87 | 30.6 | 240 | 116 |
| 4 | -15.6 | 32 | 0.0 | 60 | 15.6 | 88 | 31.1 | 250 | 121 |
| 5 | -15.0 | 33 | 0.6 | 61 | 16.1 | 89 | 31.7 | 260 | 127 |
| 6 | -14.4 | 34 | 1.1 | 62 | 16.7 | 90 | 32.2 | 270 | 132 |
| 7 | -13.9 | 35 | 1.7 | 63 | 17.2 | 91 | 32.8 | 280 | 138 |
| 8 | -13.3 | 36 | 2.2 | 64 | 17.8 | 92 | 33.3 | 290 | 143 |
| 9 | -12.8 | 37 | 2.8 | 65 | 18.3 | 93 | 33.9 | 300 | 149 |
| 10 | -12.2 | 38 | 3.3 | 66 | 18.9 | 94 | 34.4 | 310 | 154 |
| 11 | -11.7 | 39 | 3.9 | 67 | 19.4 | 95 | 35.0 | 320 | 160 |
| 12 | -11.1 | 40 | 4.4 | 68 | 20.0 | 96 | 35.6 | 330 | 166 |
| 13 | -10.6 | 41 | 5.0 | 69 | 20.6 | 97 | 36.1 | 340 | 171 |
| 14 | -10.0 | 42 | 5.6 | 70 | 21.1 | 98 | 36.7 | 350 | 177 |
| 15 | -9.4 | 43 | 6.1 | 71 | 21.7 | 99 | 37.2 | 360 | 182 |
| 16 | -8.9 | 44 | 6.7 | 72 | 22.2 | 100 | 37.8 | 370 | 188 |
| 17 | -8.3 | 45 | 7.2 | 73 | 22.8 | 110 | 43 | 380 | 193 |
| 18 | -7.8 | 46 | 7.8 | 74 | 23.3 | 120 | 49 | 390 | 199 |
| 19 | -7.2 | 47 | 8.3 | 75 | 23.9 | 130 | 54 | 400 | 204 |
| 20 | -6.7 | 48 | 8.9 | 76 | 24.4 | 140 | 60 |  |  |
| 21 | -6.1 | 49 | 9.4 | 77 | 25.0 | 150 | 66 |  |  |


| Degrees Celsius | ${ }^{\circ} \mathrm{C}=\frac{5}{9}\left({ }^{\circ} \mathrm{F}-32\right)$ | Degrees Fahrenheit | ${ }^{\circ} \mathrm{F}=\frac{9}{5}{ }^{\circ} \mathrm{C}+32$ |
| :--- | :--- | :--- | :--- |
| Degrees Kelvin | ${ }^{\circ} \mathrm{T}={ }^{\circ} \mathrm{C}+273.2$ | Degrees Rankine | ${ }^{\circ} \mathrm{R}={ }^{\circ} \mathrm{F}+459.7$ |

## Table B-8 Length Conversion

| Units of <br> Length | in. | ft. | yd. | mile | $\mathbf{m m}$ | $\mathbf{c m}$ | $\mathbf{m}$ | km |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| inch | 1 | 0.0833 | 0.0278 | - | 25.4 | 2.54 | 0.0254 | - |
| foot | 12 | 1 | 0.3333 | - | 304.8 | 30.48 | 0.3048 | - |
| yard | 36 | 3 | 1 | - | 914.4 | 91.44 | 0.9144 | - |
| mile | - | 5280 | 1760 | 1 | - | - | 1609.3 | 1.609 |
| millimeter | 0.0394 | 0.0033 | - | - | 1 | 0.100 | 0.001 | - |
| centimeter | 0.3937 | 0.0328 | 0.0109 | - | 10 | 1 | 0.01 | - |
| meter | 39.37 | 3.281 | 1.094 | - | 1000 | 100 | 1 | 0.001 |
| kilometer | - | 3281 | 1094 | 0.6214 | - | - | 1000 | 1 |
| (1 micron =0.001 millimeter) |  |  |  |  |  |  |  |  |

## Appendix C: Useful Formulas



Length of Circular Arc
$S=\varnothing \times\left(\frac{\pi}{180}\right) \times r$
$\varnothing$ in degrees
$S=\varnothing x r$
$\varnothing$ in radians

Area of Circle Sector
$A=x\left(\frac{\varnothing}{360}\right) \times \pi \times r^{2}$
$\varnothing$ in degrees
$A=x\left(\frac{\varnothing}{2}\right) \times r^{2}$
$\varnothing$ in radians

Equation of a Circle (cartesian co-ordinates)

- for a circle with center ( $j, k$ ) and radius ( $r$ )

$$
(x-j)^{2}+(y-k)^{2}=r^{2}
$$

Equation of a line (quadratic formula)
or

$$
a x+b y+c=0
$$

$$
a x^{2}+b x+c=0
$$

$x=\frac{-b \pm \sqrt{b^{2}-4 a c}}{2 a}$

## Trigonometry

$\sin \emptyset=\frac{6}{c}$
$\cos \varnothing=\frac{9}{c}$
$\tan \varnothing=\frac{\mathrm{b}}{\mathrm{a}}$
Sine Law

$$
\frac{9}{\sin A}=\frac{6}{\sin B}=\frac{c}{\sin C}=2 R
$$

Cosine Law
$C^{2}=a^{2}+b^{2}-2 a b \cos C$
$b^{2}=a^{2}+c^{2}-2 a c \cos B$
$a^{2}=b^{2}+c^{2}-2 b c \cos A$



## Appendix D: Abbreviations

| AGA | - American Gas Association |
| :---: | :---: |
| ANSI | - American National Standards Institute |
| API | - American Petroleum Institute |
| ASME | - American Society of Mechanical Engineers |
| ASTM | - American Society for Testing and Materials |
| AWWA | - American Water Works Association |
| BOCA | - Building Officials and Code Administrators |
| BS | - British Standards Institution |
| CPVC | - Chlorinated poly (vinyl chloride) plastic or resin |
| CS | - Commercial Standard, see Product Standard |
| CSA | - Canadian Standards Association |
| DR | - Dimension Ratio |
| DIN | - German Industrial Norms |
| FHA | - Federal Housing Administration or Farmers Home Administration |
| HDB | - Hydrostatic design basis |
| HDS | - Hydrostatic design stress |
| IAPD | - International Association of Plastics Distributors |
| IAPMO | - International Association of Plumbing and Mechanical Officials |
| IPC | - International Plumbing Code |
| ISO | - International Standards Organization |
| JIS | - Japanese Industrial Standards |
| NSF | - National Sanitation Foundation International |
| PPI | - Plastics Pipe Institute |
| PS | - Product Standard when in reference to a specification for plastic pipe and fittings. These specifications are promulgated by the U.S. Department of Commerce and were formerly known as Commercial Standards. |
| PSI | - Pounds per square inch |
| PSIG | - Gage pressure in pounds per square inch |
| PVC | - Poly (vinyl chloride) plastic or resin |
| RVCM | - Residual Vinyl Chloride Monomer |
| SCS | - Soil Conservation Service |
| SDR | - Standard Dimension Ratio |
| SI | - International System of Units |
| SPI | - Society of the Plastics Industry, Inc. |
| UPC | - Uniform Plumbing Code |
| USASI | - United States of America Standards Institute (formerly American Standards Association) |
| WOG | - Water, Oil, Gas |

## Appendix E: Tables and Figures

Table 1 Percent (\%) Deflection for IPEX Centurion Pressure Pipe
Table 2 Q-Line Flow Rates
Table 3 Summary of Properties
Table 4 Temperature Effects on PVC Pressure Pipe
Table 5 AWWA C900 Pressure Classes
Table 6 Hazen-Williams "C"-Factors
Table 7 Thrust Developed per 100 psi Pressure (Ibs. force)

Figure 1 Stress Regression Line - 12454
Figure 2 Pipe Material
Figure 3 Resulting Cyclic-Failure Curves for PVC
Figure 4 Pipeline Profile

## Blue Brute Fittings

Blue Brute fittings are injection molded and are even tougher than the pipe. Injection molded Blue Brute fittings have a wall thickness $125 \%$ larger than SDR18 pipe, and custom-made fabricated fittings are wrapped with a tough layer of fiberglass for extra protection.


## Corrosion-Proof Performance

Blue Brute systems are immune to corrosion from aggressive soils and galvanic action.

## Superior Hydraulics

The glass-like finish of PVC reduces friction losses and eliminates the tuberculation common in iron pipes. As a result, pumping costs are reduced and water quality is maintained.

## Strength

A thicker bell that results in a more robust fitting.

## Gaskets Options

All Blue Brute fittings are shipped with standard gaskets that accept cast-iron-sized PVC pipe. Transition gaskets for IPS-sized pipe are an option for all sizes. For applications where fittings must be buried in soil with hydrocarbon contamination, Nitrile gaskets are available.

## Saves Time \& Money

A consistent O.D. for each size, simplifying the restraint selection. Each fitting is labeled with the O.D. information for easy identification and restraint selection.

## Third-party Certification

All IPEX municipal systems are third-party certified as applicable. In addition, IPEX Centurion and Blue Brute systems have Factory Mutual approval and Underwriter's Laboratories (ULI and ULC) listings.

## MUNICIPAL PRESSURE PIPING SYSTEMS

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חEய PROロUCT SHOUCASE


\title{
IPEX offers "more robust" fabricated fittings in sizes 4" to 16" for use on C900 and C905 pipe
}

IPEX is now offering a new and improved fabricated fitting for Blue Brute and Centurion pressure piping systems. Designed with a thicker bell, the standardized fitting provides a more robust bell than any other fabricated C900/C905 fitting currently offered in North America.

The new bells also have the same O.D. and thickness as the bells on Blue Brute and Centurion pipes providing a consistent O.D. throughout the entire offering.

\section*{FEATURES AND BENEFITS:}
- A thicker bell that results in a more robust fitting.
- A consistent O.D. for each size, simplifying the restraint selection.
- Each fitting is labeled with the O.D. information for easy identification and restraint selection.

\section*{A -PEx (1)}

Products are manufactured by IPEX Inc. and distributed in the United States by IPEX USA LLC. Blue Brute \({ }^{\bullet}\) \& Centurion \({ }^{\ominus}\) are trademarks of IPEX Branding Inc.

\section*{CLASSIFICATIONS:}
- PVC Pressure Systems manufactured to the performance requirements of AWWA and CSA Standards

\section*{STANDARD PRODUCT OFFERING}

4" ( 100 mm ) to \(16^{\prime \prime}\) ( 400 mm ) - PR 235psi (DR18)
Note: Other DR's and sizes up to 48" (1200mm) are available upon request.


\section*{IPEX Centurion}
\(14^{\prime \prime}-48^{\prime \prime}(350 \mathrm{~mm}-1200 \mathrm{~mm})\)
IPEX Centurion extends the corrosion-free benefits of Blue Brute to larger diameters of pipe and new applications. The versatility and ease of installation of IPEX Centurion is unmatched - shop drawings are eliminated and costly and difficult to install corrosion protection can be eliminated. In addition, unlike HDPE or concrete pressure pipe, every length of IPEX Centurion is tested to double its pressure rating.


\section*{COMPATIBLITY}

IPEX Centurion is manufactured with a cast iron outside diameter (CIOD) so it is compatible with much of the existing older infrastructure of iron pipes. In addition, IPEX Centurion can be field cut, which means unexpected changes in the field can be accommodated quickly, without having to wait for new shop drawings. IPEX Centurion Fittings are manufactured using sections of AWWA C905 pipe, overwrapped with a layer of fibre reinforced plastic (FRP). While IPEX Centurion is compatible with iron fittings, IPEX recommends the use of IPEX Centurion fittings exclusively with IPEX Centurion pipe.


\section*{IPEX Centurion \({ }^{\circledR}\) and Blue Brute \({ }^{\circledR}\) Pressure Piping Systems}

\author{
PVC Pressure Systems manufactured to AWWA and CSA Standards
}

IPEX Centurion \({ }^{\circledR} 14\) - 48 " ( 350 mm - 1200mm), AWWA C905 and CSA Standards

Blue Brute \({ }^{\circledR} 4^{\prime \prime}-12^{\prime \prime}(100 \mathrm{~mm}-300 \mathrm{~mm})\), AWWA C900 and CSA Standards

Designed for municipal applications, IPEX Centurion \({ }^{\circledR}\) and Blue Brute \({ }^{\circledR}\) systems deliver superior strength with corrosion resistant performance and the ability to flex without damage.

IPEX municipal pressure piping systems are made with a highstrength, high-impact PVC compound, allowing them to perform even under high traffic loads and deep burial conditions.

\section*{TPEXGENIURION}

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Products are manufactured by IPEX Inc. and distributed in the United States by IPEX USA LLC.
Centurion \({ }^{\oplus}\) and Blue Brute \({ }^{\oplus}\) are trademarks
of IPEX Branding Inc.

For applications involving potable water, irrigation systems, or sewage forcemains, IPEX municipal systems offer the lowest break rate of any pipe material.

Blue Brute fittings are injection molded and are even tougher than the pipe. Injection molded Blue Brute fittings have a wall thickness 125\% larger than SDR18 pipe, and custom-made fabricated fittings are wrapped with a tough layer of fiberglass for extra protection.

Proven in tough North American climates for over 50 years, IPEX PVC pipe, fitting and valve systems have an established track record of performance.

\section*{ㅔ ( (2) (1) (1) )}

US Customers call IPEX USA LLC
Toll Free: (800) 463-9572
www.ipexamerica.com

Key features include:
- Corrosion-proof Performance

IPEX Centurion and Blue Brute systems are immune to corrosion from aggressive soils and galvanic action.
- Superior Hydraulics

The glass-like finish of PVC reduces friction losses and eliminates the tuberculation common in iron pipes. As a result, pumping costs are reduced and water quality is maintained.

Cast Iron Outside Diameter (CIOD)
Blue Brute and IPEX Centurion systems are manufactured with a cast iron outside diameter (CIOD). This is compatible with waterworks valves, appurtenances and restrainers.
- Bottle-tight Joints, Removable Gaskets

IPEX's patented gasket system not only withstands many times the rated system pressure, but also withstands full vacuum pressures. The unique removable gasket system allows special oil-resistant (nitrile) gaskets to be easily installed when working in contaminated soils.
- Third-party Certification

All IPEX municipal systems are third-party certified as applicable. In addition, IPEX Centurion and Blue Brute systems have Factory Mutual approval and Underwriter's Laboratories (ULI and ULC) listings.

Pressure Classes vs. Pressure Ratings
Water distribution systems normally consist of smaller diameter pipes 4" - 12" (100 mm 300 mm ) with many connections, taps, bends, valves, hydrants and other appurtenances. As a result, pipes in this size range are referred to by their pressure class. Pressure classes are defined in AWWA C900 and include a 2.5:1 safety factor for pressure, and a \(2 \mathrm{ft} / \mathrm{s}\) \((0.6 \mathrm{~m} / \mathrm{s})\) guideline for surge allowance. IPEX's Blue Brute adheres to this standard.

Conversely, larger diameter transmission pipes 14" - 48" ( \(350 \mathrm{~mm}-1200 \mathrm{~mm}\) ) are grouped by pressure rating. A pressure rating as defined in AWWA C905 includes a 2:1 safety factor, which is more appropriate for larger diameter pipes. IPEX Centurion conforms to this standard.

AWWA C900 governs smaller water distribution systems pipes, while AWWA C905 governs larger diameter transmission pipe. All sizes adhere to the CSA B137.3 standard which recommends a 2:1 safety factor for both distribution and transmission applications.

Pressure Classes and Ratings
Note that these classes and ratings are extremely conservative. For instance, the minimum burst pressure for IPEX DR 18 pipe is 755 psi, but the pipe routinely withstands over 1000 psi.
\begin{tabular}{|c|c|c|}
\hline Dimension Ratio & Pressure Class & Pressure Rating \\
\hline 14 & 200 & 305 \\
\hline 18 & 150 & 235 \\
\hline 25 & 100 & 165 \\
\hline 32.5 & N/A* & 125 \\
\hline 41 & N/A* & 100 \\
\hline 51 & N/A* & 80 \\
\hline *Not manufactured in \(4^{\prime \prime}-12^{\prime \prime}(100 \mathrm{~mm}-300 \mathrm{~mm})\) sizes \\
\hline
\end{tabular}

\section*{IPEX Fusible \\ NEW}

IPEX has introduced new Fusible Brute and Fusible Series PVC pipes. By combining the mechanical properties of PVC with an innovative, patentpending butt fusion process, IPEX provides the only available method of installing a continuous, monolithic, fully restrained PVC pipe system. Capable of being used in a variety of trenchless or conventional direct bury applications, Fusible \(\mathrm{PVC}^{\mathrm{TM}}\) pipe systems have been installed at numerous sites throughout the United States, Canada and Mexico for both pressure and non-pressure installations in the water and sewer industries.


With PVC's proven long service life, Fusible Brute (CIOD) and Fusible Series (IPS) pipes are available in sizes ranging from \(100 \mathrm{~mm}\left(4^{\prime \prime}\right)\) to \(900 \mathrm{~mm}\left(36^{\prime \prime}\right)\) with larger sizes in development. The proprietary PVC formulation, fusion process as well as our licensing and training program allow for the consistent, reliable fusion of Fusible Brute and Fusible Series pipes to create piping systems of unparalleled strength.

\section*{ADVANTAGES}

> PVC is the most widely installed material in water systems today Greater pull force rating than HDPE and greater pull force rating than other PVC systems
> Lower installation costs versus HDPE due to lighter weight and reduced OD dimensions
> Creates gasket-free joints
> Has excellent abrasion and scratch-resistant properties
> Continuous pull-in lengths of over 1500 meters have been achieved
> Higher flow rates
> Connect directly to existing PVC systems for material consistency Uses standard CIOD or IPS fittings
> Creates monolithic, fully-restrained pipe systems

\section*{Fusible PVC' Pipe for Iremahleass Andierations}


M U N I C I P AL S Y S TEMS

FUSIBLE PVCTM PIPE FOR HDDAND OTHER TRENCHLESS APPLICATIONS
- 100 mm - \(900 \mathrm{~mm}\left(4^{\prime \prime}-36\right.\) ") CIOD \& IPS Sizes
- \(12.2 \mathrm{~m}(40 \mathrm{ft})\) lengths

We build tough products for tough environments \({ }^{\circledR}\)

\section*{IPEX FUSible}

\section*{GO TRENCHLESS WITH PVC™}


IPEX has introduced new Fusible Brute \({ }^{\text {TM }}\) and Fusible Series \({ }^{\text {TM }}\) PVC pipes. By combining the mechanical properties of PVC with an innovative, patent-pending butt fusion process, IPEX provides the only available method of installing a continuous, monolithic, fully restrained PVC pipe system. Capable of being used in a variety of trenchless or conventional direct bury applications, Fusible PVC \({ }^{\text {TM }}\) pipe systems have been installed at numerous sites throughout the United States, Canada and Mexico for both pressure and non-pressure installations in the water and sewer industries.

With PVC's proven long service life, Fusible Brute (CIOD) and Fusible Series (IPS) pipes are available in sizes ranging from 100 mm (4") to 900 mm (36") with larger sizes in development. The proprietary PVC formulation, fusion process as well as our licensing and training program allow for the consistent, reliable fusion of Fusible Brute and Fusible Series pipes to create piping systems of unparalleled strength.

\section*{The Fusion Process}

Fusible Brute and Fusible Series PVC pipe have distinctive properties allowing for full strength butt fusion joints. While other thermoplastic materials have been fused routinely, the patent-pending fusion process incorporates a proprietary PVC formulation and a
unique combination of heat, pressure and time, using slightly modified standard industry fusion machines.

All fusion times are comparable to other thermoplastic materials. All joints are fully restrained. Testing performed in accordance with ASTM D-638 methods, demonstrates that the tensile strength of the fused joint equals the tensile strength of the pipe.

\section*{Installation Methods:}
- Horizontal Directional Drilling (HDD)
- Sliplining
- Pipe Bursting
- Direct Bury

\section*{Applications:}
- Water Mains
- Sanitary Sewers
- Process and Raw Water
- Reclaimed Water
- Storm Drains


\section*{Pipe Specifications:}
- Meets CSA Bl37.3, AWWA C900, AWWA C905, NSF-61 and ASTM cell classification 12454
- Available in CIOD and IPS sizes
- 12.2 m (40') lengths

FUSiBLE BRUTE FUSiBLE SERIES

\section*{PRESSURE RATINGS}

FUSIBLE BRUHE (CIOD)
\begin{tabular}{|c|c|}
\hline Dimension Ratio & Pressure (psi) \\
\hline DR 14 & 305 \\
DR 18 & 235 \\
DR 25 & 165 \\
DR 32.5 & 125 \\
DR 41 & 100 \\
\hline
\end{tabular}

FUSiBLE SERIES (IPS)
\begin{tabular}{|c|c|}
\hline Dimension Ratio & Pressure (psi) \\
\hline DR 21 & 200 \\
\hline DR 26 & 160 \\
\hline
\end{tabular}

\section*{faATURES \& BENEFITS}
\(\checkmark\) PVC is the most widely installed material in water systems today
\(\checkmark\) Greater pull force rating than HDPE
\(\checkmark\) Greater pull force rating than other PVC systems
\(\checkmark\) Reduced wall thickness relative to HDPE yields more flow and less material for given pressure class
\(\checkmark\) Lower installation costs versus HDPE due to lighter weight and reduced OD dimensions
\(\checkmark\) Creates gasket-free joints
\(\checkmark\) Has excellent abrasion and scratch-resistant properties
\(\checkmark\) Continuous pull-in lengths of over 1500 meters have been achieved

\section*{ADVANTAGES}
- Higher flow rates
- Connect directly to existing PVC systems for material consistency
- Uses standard CIOD or IPS fittings
- Creates monolithic, fully-restrained pipe systems

\section*{PROJECTS}
unney's Pasture Potable Water Main, Ottawa, Ontario
305 m ( 1,000 LF) of 300 mm (12") DR18,
110 m ( 360 LF ) of 400 mm (16") DR25


Fusion Set-Up


Cold Weather Fusion at \(-14^{\circ} \mathrm{C}\left(6^{\circ} \mathrm{F}\right)\)

Potable Water Main, Burlington, Ontario \(609 \mathrm{~m}(2,000\) LF) of 200 mm (8") DR14, 183 m ( 600 LF ) of 200 mm (8") DR14


Insertion into Entrance


Expansion Head \& Pull Head

New Supply Pipeline, Sooke, BC
\(3,140 \mathrm{~m}\) ( 10,300 LF) of 600 mm (24") DR32.5


4m (14 LF) Right of Way


Pipe Pulled In

Distribution Line for City of Richmond, Richmond, BC 700 m ( \(2,300 \mathrm{LF}\) ) of 150 mm ( \(6^{\prime \prime}\) ) DR18


Fusing on Street


HDD Pipe Insertion

\section*{TerraBrute CR mew}
\(4^{\prime \prime}-12^{\prime \prime}(100 \mathrm{~mm}-300 \mathrm{~mm})\)
Engineered for Horizontal Directional Drilling (HDD) and other trenchless applications, TerraBrute® CR is a \(100 \%\) non-metallic, AWWA C900 PVC pressure pipe system. Noncorroding and installation friendly, TerraBrute CR allows you to standardize on PVC throughout your potable water and sewer infrastructure. Whether you're using open-cut on trenchless methods, there are no more problems matching materials and couplings. No more butt fusion equipment headaches. No more surprises.


TerraBrute CR's patented non-metallic "ring-and-pin" gasketed joint design outperforms all other restrained PVC pipe joints on the market, providing more than twice the pull strength of other HDD systems - up to \(120,000 \mathrm{lbs}\). for \(300 \mathrm{~mm} / 12^{\prime \prime}\) pipe. Unlike competing square-shoulder designs, TerraBrute CR's rounded bell shoulders slide by roots, rocks and other debris that can protrude into the borehole. And unlike HDPE, TerraBrute CR requires no relaxation time before installation of fittings or services.

\section*{Standards}

\section*{AWWA C900}

TerraBrute is made with pipe conforming to AWWA C900, however once the pipe is grooved on the spigot end its dimensions do not match those published in the C900 standard. Because of this small dimensional difference the pipe, once grooved, does not strictly conform to the C900 standard. It is important to note however, that TerraBrute is subjected to the same testing program as IPEX's Blue Brute (C900) pipe.

CSA B137.3
TerraBrute is made from stock certified to CSA B137.3.
NQ 3624-250
Factory Mutual and Underwriter's Laboratories TerraBrute is made from starting stock that is Factory Mutual, ULC and ULI Approved

\section*{PCMFing Snsemsion Hillanil Char Trentiless Anpiriaicins}

\section*{TerraBute ©}


M U N I C I P A L S Y S TEM S

AWWA C900 PRESSURE PIPE SYSTEMS FOR POTABLE WATER AND SEWER APPLICATIONS
\(100 \mathrm{~mm}-300 \mathrm{~mm}\)
\(4^{\prime \prime}-12\) "

\section*{TERRABRUTE \({ }^{\oplus}\) CR TRENCHLESS THE MISSING LINK IN YOUR TOTAL PVC PIPING SYSTEM}

\section*{TOTAL PVC PIPING SYSTEM ENGINEERED FOR HDD}

Engineered for Horizontal Directional Drilling (HDD) and other trenchless applications, TerraBrute \({ }^{\oplus}\) CR is a 100\% non-metallic, AWWA C900 PVC pressure pipe system. Non-corroding and installation friendly, TerraBrute CR allows you to standardize on PVC throughout your potable water and sewer infrastructure. Whether you're using open-cut or trenchless methods, there are no more problems matching materials and couplings. No more butt fusion equipment headaches. No more surprises.

\section*{HIGHEST PULL STRENGTH AVAILABLE}

Developed in consultation with leading trenchless technology research experts, and rigorously tested in the field, TerraBrute CR trenchless PVC pressure pipe easily withstands the high tensile and bending forces that occur during HDD and other types of trenchless installation.

TerraBrute CR's patented non-metallic "ring-and-pin" gasketed joint design outperforms all other restrained PVC pipe joints on the market, providing more than twice the pull strength of other HDD systems - up to 120,000 lbs. for \(300 \mathrm{~mm} / 12^{\prime \prime}\) pipe. Unlike competing square-shoulder designs, TerraBrute CR's rounded bell shoulders slide by roots, rocks and other debris that can protrude into the borehole. And unlike HDPE, TerraBrute CR requires no relaxation time before installation of fittings or services.


These ultimate load values were calculated using a semi-empirical design method derived at the University of Western Ontario and verified by laboratory testing. A safety factor of 2:1 should be applied to account for the combined tensile and bending loads associated with HDD applications.
\begin{tabular}{|c|c|c|c|c|c|c|}
\hline \multicolumn{7}{|c|}{ Dimensions of TerraBrute CR Pipe } \\
\hline \multicolumn{2}{|c|}{\begin{tabular}{c} 
Nominal \\
Diameter
\end{tabular}} & \begin{tabular}{c} 
Pressure Rating \\
(2:1 safety factor)
\end{tabular} & \begin{tabular}{c} 
Max Outside \\
Diameter \\
(Bell OD)
\end{tabular} & \multicolumn{2}{c|}{\begin{tabular}{c} 
Avg Internal \\
Diameter
\end{tabular}} \\
mm & in & psi & mm & in & mm & in \\
\hline 100 & 4 & 305 & 165 & 6.49 & 104 & 4.09 \\
\hline 150 & 6 & 305 & 230 & 9.06 & 149 & 5.87 \\
\hline 200 & 8 & 235 & 288 & 11.33 & 204 & 8.03 \\
\hline 250 & 10 & 235 & 355 & 14.00 & 250 & 9.84 \\
\hline 300 & 12 & 235 & 416 & 16.36 & 297 & 11.69 \\
\hline
\end{tabular}

TerraBrute CR's larger internal diameters, compared to HDPE pipe, provide the same hydraulic performance usually with one size smaller pipe, saving on material costs.

TerraBrute CR is the result of many years of research into the use of PVC pipes in HDD applications. The new noncorroding, locking joint design enables TerraBrute CR to enter new applications while maintaining the high tensile strength and bending radius of the original TerraBrute.

Dr. Erez Allouche, Louisiana Tech University

\section*{CORROSION RESISTANT}

The new, non-metallic, "ring-and-pin" configuration of TerraBrute CR PVC pressure pipe offers complete corrosion resistance. The plastic "ring" is designed as two half rings for ease of installation and comes complete with the "pins" ready for insertion creating a strong, locking joint.

\section*{PROVEN PERFORMANCE}

Pressure rated in excess of 200 psi, TerraBrute CR delivers the superior strength and corrosion resistance you've come to expect from our Blue Brute pressure pipe, along with the ability to absorb the underground shear and flexure stresses that occur in buried applications.

\section*{PROVEN COMPATIBILITY}

TerraBrute CR trenchless PVC pipe is designed for total compatibility with your municipal system. Connections can be made with standard PVC CIOD fittings, direct tapped couplings or standard service saddles. Repair and handling techniques are the same as for any AWWA PVC pressure pipe.

\section*{PROVEN JOINING SYSTEM}

Based on our gasketed bell and spigot design, proven through years of service in the field, the TerraBrute CR joint is rated at many times the pressure rating of the pipe. And unlike competing coupling joints, the TerraBrute CR joint has been specially engineered to deliver the highest pull strength safety factors in the industry for HDD applications.

\section*{FAST AND EASY JOINT ASSEMBLY}

Unlike butt fusion or electrofusion joining methods used with HDPE pipe, TerraBrute CR requires no expensive equipment or special installer training. Because pipe segments are assembled during pullback operations, pipe stringing is eliminated. Assembly time for a \(300 \mathrm{~mm} / 12^{\prime \prime}\) TerraBrute CR joint is typically less than five minutes.

\section*{TerraBrute CR}

\section*{IDEAL TERRABRUTE CR APPLICATIONS}

\section*{BRIDGE CROSSINGS}

TerraBrute CR's unique "new non-metallic ring-and-pin" joint design provides for easy installation in non-HDD applications where traditional butt fusion techniques would be difficult - such as this span of suspended pressure pipe installed beneath a busy roadway bridge.


\section*{ROAD CROSSINGS}

TerraBrute CR is ideally suited for short drilling projects where existing structures cannot be disturbed - such as under busy highways, roads and intersections where you connect to PVC pipes.


\section*{URBAN CENTERS}

Because TerraBrute CR can be assembled segmentally just before entering the borehole, projects take up less space in restricted urban areas, compared to the long strings of pipe typical with conventional PVC and HDPE installations.


\section*{JOINT ASSEMBLY}

Lubricate and

\(\square\)assemble joint as for standard PVC pressure pipe.

Insert spigot up to the insertion
line, aligning the internal ring and the pin holes.


One Ring at a time, place ring over pin holes and tap pins in until they bottom out on the inner groove.



CIOD \& IPSOD: \(4^{\prime \prime}-12^{\prime \prime}(100 \mathrm{~mm}-300 \mathrm{~mm})\)
Imagine a pipe with all the benefits associated with conventional PVC, yet dramatically stronger and more impact resistant.


Bionax is a molecularly-enhanced PVC pipe designed for water mains, sewage forcemains, irrigation lines and industrial process piping. Made from biaxially-oriented PVC material, Bionax has almost double the strength of conventional PVC and three times the impact absorption capability. Using a revolutionary new orientation process, this ultra hightech process orients the PVC molecules both in the axial and circumferential directions (biaxial orientation). The result is a pipe with enhanced toughness and flexibility. Bionax is specially engineered to withstand the rigors of today's installations. With less construction inspection, and less regular maintenance, the market is calling for a pipe that is more robust, stronger and easier to install. Bionax delivers on all three counts.

\section*{The First Biaxially-Oriented PVC Pipe for Municipal Applications}

Bionax's biaxial orientation dramatically enhances the pipe properties that are important to municipal designers:
- Larger internal diameters increase flow rates and reduce pumping costs
- Higher cyclic fatigue resistance for forcemain and irrigation applications
- Reduced surge pressure

\section*{A Remolicionin PVCI Iutimess \& flexitiliy}


M U N I C I P A L S Y S TEM S

MOLEGULARLY ENHANGED PVCO PRESSURE PIPEFOREJNDERGROUND WATEREND-SEWER APPLICATIONS
- 4"-12" ( \(100 \mathrm{~mm}-300 \mathrm{~mm}\) ) CIOD \& IPSOD Sizes
- Operating Pressures 235psi CIOD, 160 psi IPSOD

We build tough products for tough environments

\section*{BiONAX}

\section*{A REVOLUTION IN STRENGTH, TOUGHNESS AND FLEXIBILITY}

Imagine a pipe with all the benefits associated with conventional PVC, yet dramatically stronger and more impact resistant.
Introducing Bionax, a molecularly-enhanced PVC pipe designed for water mains, sewage forcemains, irrigation lines and industrial process piping. Made from biaxially-oriented PVC material, Bionax has almost double the strength of conventional PVC and three times the impact absorption capability. While millions of feet of earlier versions of oriented PVC have been installed, Bionax is manufactured using a revolutionary new orientation process, previously unavailable in North America. This ultra high-tech process orients the PVC molecules both in the axial and circumferential directions (biaxial orientation), resulting in a pipe with enhanced toughness and flexibility even when compared to earlier versions of oriented PVC.

Bionax is specially engineered to withstand the rigors of today's installations. With less construction inspection, and less regular maintenance, the market is calling for a pipe that is more robust, stronger and easier to install. Bionax delivers on all three counts.

\section*{The First Biaxially-Oriented PVC Pipe for Municipal Applications}

Bionax's biaxial orientation dramatically enhances the pipe properties that are important to municipal designers:

Larger internal diameters increase flow rates and reduce pumping costs
- Higher cyclic fatigue resistance for forcemain and irrigation applications

Things are not always perfect in the field. Pipe can be impacted by equipment, bedded with sharp stones and boulders, or even pierced by directional drilling equipment. Bionax is designed to withstand even the most violent impact events, and if pierced by a directional drill or "torpedo" type piercing tool, will exhibit only a localized failure. The unique layered material structure that resists impacts also stops cracks before they propagate.
- Reduced bend radius when compared


\section*{Impact Resistant}

With three times the impact strength of regular PVC, Bionax can handle the most punishing storage, handling and construction site conditions.


Tapping Strength
Bionax's unique structural design
Bionax's unique structural design
allows tapping holes to be drilled close together without the risk of splitting or cracking.



\section*{Pressure Tough}

Bionax's unique molecular reinforcement gives it the ability to withstand extreme internal pressures and deform instead of failing.


\section*{Excellent Hydraulics}

Bionax's smooth inside surface and larger ID means less friction headloss versus other materials. The reduced pumping costs and energy use are good for the environment.


The Green Solution
Bionax has the lowest embodied energy per metre than any other piping material. Taking less energy to manufacture, Bionax has the lowest carbon footprint of any piping product available.


\section*{Lightweight \& Easier to Handle}
\(40 \%\) lighter than conventional PVC, Bionax is safer and easier to carry. This means less equipment is required and installation is fast and efficient. Bionax's increased flexibility means a reduced bending radius that allows it to fit around gradual curves. In fact, Bionax is so light and flexible that several joined lengths can be lifted as a single unit and installed in a trench, further speeding installation.

\section*{Reduced Maintenance \& Pumping Costs}

Bionax's increased strength allows higher inside diameters for the same pressure rating, reducing pumping costs. Bionax's smooth inside surface maintains its excellent hydraulic properties virtually forever with extremely low maintenance costs, saving energy associated with pumping and maintaining its superior flow profile.

\section*{Manufacturing Consistency \& Quality}

Bionax's ultra high-tech manufacturing process ensures that the pipe will meet the toughest standards. In fact, the initial stock pipe must be flawless in order to survive the orientation process - in essence, the process acts as its own quality control. Bionax is \(100 \%\) I.D. and O.D. controlled, meaning that its tolerances are much tighter than conventional pipe.

\section*{Joining Methods}

Bionax's standard joining method uses easy-to-assemble gasketed joints. No special training is required to install Bionax as the procedure is virtually identical to standard
 PVC pipe. In addition, research has shown that Bionax can be successfully solvent cemented for above ground applications. This brings the benefits of a super-impact resistant pipe to an entirely new set of applications.

\section*{Integrated Total PVC Solutions}

Typical of any IPEX piping system, Bionax offers a totally-integrated solution. The entire end-to-end system integrates seamlessly and is compatible with regular C900 and C907 fittings. When you purchase Bionax, you get everything - all the pipe and fittings - you need to get the job done. And since it comes from IPEX, you also get the peace of mind knowing your system is supplied by a single trusted and accountable source who is guaranteed to stand behind you and your piping system.


\section*{APPLCATIONS}

\section*{Water Mains}

Sewage Force Mains
Irrigation Lines
Industrial Process Piping

\title{
BiONAメ MOLECULARLY ENHANCED PVCO PIPE
}

While biaxial orientation isn't a new process, it's been difficult to produce efficiently and reliably in high volumes. Thanks to a breakthrough in innovative manufacturing, IPEX now uses the most advanced process in the plastics industry to biaxially orient PVC molecules and produce the lightest, strongest pipe available.
In the past, oriented PVC was expanded in a mold, resulting in orientation in only one direction. Now biaxial orientation is achieved by stretching pipe over a mandrel at tightlycontrolled temperatures and stress levels. The result is a pipe with dramatically-enhanced properties both in the circumferential direction (increased hoop stress capability) and in the longitudinal direction (higher impacts, point loading and lower bending radius). More importantly, Bionax's manufacturing process consistently maintains these qualities with a continuous process, rather than using older batch processing technology.

While these cutting-edge manufacturing techniques are expensive, they result in the strongest, toughest and most consistent high-quality pipe available on the market today.


Stretching regular PVC pipe biaxially in both the hoop and axial directions-lengthways and sideways-over a mandrel after the pipe is extruded dramatically improves the performance of PVC material.


Regular PVC is manufactured in a single layer.

When PVC pipe is extruded in the traditional way, a more or less spherical molecular structure results, requiring thicker walls to provide the necessary strength.


Because they're unaligned, the molecules within regular PVC react to force in a general, haphazard direction.


Due to biaxial molecular orientation during the manufacturing process, thin stratified layers are formed within the PVCO, resulting in higher impact strength even under extreme pressure.


As the PVC is stretched, so are the spherical molecules, allowing more of these elongated molecules to fit into a single layer than regular PVC. This gives the material a higher molecular density and makes it tougher.


Biaxial stretching creates a molecular orientation in which the molecules can be aligned in the direction of the expected load, resulting in superior force resistance.

\section*{ZiONA×}

ClOD PIPE
\begin{tabular}{|c|c|c|c|c|c|}
\hline Nominal Sizes & 4"(100mm) & 6"(150mm) & 8"(200mm) & \(10 \mathrm{Cl}(250 \mathrm{~mm})\) & 12 "(300mm) \\
\hline Outside Diameter & 4.80 " 122 mm ) & 6.90 " 1775 mm ) & \(9.05{ }^{\prime \prime}(230 \mathrm{~mm})\) & 11.10 "(282mm) & 13.20 "(335mm) \\
\hline Pressure Rating & \multicolumn{5}{|c|}{235 psiat \(73{ }^{\circ} \mathrm{F}\)} \\
\hline \multicolumn{6}{|c|}{Available in \(20 \mathrm{ft}\). lengths} \\
\hline
\end{tabular}
\begin{tabular}{|c|c|c|c|c|c|}
\hline Nominal Sizes & 4"(100mm) & \(\mathrm{f}^{\prime \prime}(150 \mathrm{~mm})\) & 8"(200mm) & \(10 \mathrm{Cl}(250 \mathrm{~mm})\) & 12 "(300mm) \\
\hline Outside Diameter & \(4.500^{\prime \prime}(114 \mathrm{~mm})\) & \(6.633^{\prime \prime}(168 \mathrm{~mm})\) & \(8.633^{\prime \prime}(219 \mathrm{~mm})\) & 10.75 "(273mm) & 12.75 " 324 mm ) \\
\hline Pressure Rating & \multicolumn{5}{|c|}{160 psiat \(73^{\circ} \mathrm{F}\)} \\
\hline \multicolumn{6}{|c|}{Available in 20 ft . lengths} \\
\hline
\end{tabular}

\section*{MUNICIPAL PRESSURE PIPING SYSTEMS}

\section*{FFGOLET INFEFMFTION EILLETIN}

\section*{IPEX CycleTough \({ }^{\circledR}\) IPS Piping Systems}

PVC Pressure Systems manufactured to CSA and ASTM Standards

CycleTough \({ }^{\text {TM }}\) Pipe
( 40 mm - 600 mm ), CSA B137.3, ASTM D2241

Injection Molded Fittings ( 40 mm - 200 mm ), CSA B137.3, various ASTM Standards

CycleTough \({ }^{\text {TM }}\) IPS piping systems are specifically designed for irrigation systems and sewer forcemains. The constant cyclic surging that is associated with these applications demands a tough pipe, and more importantly, a specially

\section*{GycheTouen}

Unlike many competing fittings, CycleTough fittings are made with a long-life compound that extends service by \(25 \%\). In addition, CycleTough fittings have been engineered using the latest techniques in Finite Element Analysis (FEA), ensuring problem-free performance for the long haul.

IPEX CycleTough systems are made with the same high-impact, engineered compound as our Blue Brute \({ }^{T M}\) systems, and are tested to maintain the same high standards.

Proven in tough North American climates for over 50 years, IPEX PVC pipe systems have an established track record of performance.

\section*{Key features include:}
- High Impact Strength

CycleTough systems have a \(2: 1\) safety factor for long-term pressures, and over 3.2:1 for temporary surges. CycleTough systems easily withstand surges over 600 psi .

\section*{- Fittings Engineered Tough}

CycleTough fittings are engineered for versatility and reliability. Their unique design features extra material added for reinforcement to withstand the stresses imposed by tough irrigation and forcemain applications.
- Iron Pipe Size Outside Diameters (IPSOD)

CycleTough systems are made with an IPSOD, which is the same outside diameter configuration as schedule piping and most steel process piping.
- Bottle-tight Joints, Removable Gaskets

IPEX's patented gasket system not only withstands many times the rated system pressure, but also withstands full vacuum pressures. The unique removable gasket system allows special oil-resistant (nitrile) gaskets to be easily installed when working in contaminated soils.

Note: Gaskets on molded fittings are not removable

\section*{- Third-party Certification}

All CycleTough systems are certified to CSA B137.3. Third-party certification verifies a system will perform as expected, meeting all applicable standards.

\section*{Pressure Ratings and Burst Pressures}
\begin{tabular}{|c|c|c|c|}
\hline \begin{tabular}{c} 
Size Range \\
\((\mathrm{mm})\)
\end{tabular} & \begin{tabular}{c} 
Dimension \\
Ratio
\end{tabular} & \begin{tabular}{c} 
Pressure \\
Rating \((\mathrm{psi})\)
\end{tabular} & \begin{tabular}{c} 
Minimum Burst \\
Pressure (psi)
\end{tabular} \\
\hline \(40-600\) & 21 & 200 & 640 \\
\hline \(40-600\) & 26 & 160 & 512 \\
\hline \(75-600\) & 32.5 & 125 & 406 \\
\hline \(100-600\) & 41 & 100 & 319 \\
\hline
\end{tabular}

\section*{Why CycleTough for Cyclic Applications?}

Current research shows that PVC pipe has a virtually unlimited lifespan under some of the most demanding cyclic conditions. While the pipe is inherently 'CycleTough', fittings are subject to a variety of different stresses that can easily damage a conventionally designed product. CycleTough injection molded fittings have been specifically designed for highpressure cyclic applications using the latest engineering methods, and extensive computer modeling. While other PVC fittings may not be up to the task, CycleTough fittings were designed for it, with the right amount of material in the right places. That is why CycleTough fittings look different from other PVC fittings on the market, they are made for tough applications.

\section*{Cycle Tough}

Pipe: \(100 \mathrm{~mm}-400 \mathrm{~mm}\) - Injection Molded Fittings: \(\mathbf{4 0 m m}-200 \mathrm{~mm}\)
CycleTough \({ }^{\text {TM }}\) IPS piping systems are specifically designed for irrigation systems and sewer forcemains. The constant cyclic surging that is associated with these applications demands a tough pipe, and more importantly, a specially engineered fitting.


Unlike many competing fittings, CycleTough fittings are made with a longlife compound that extends service by \(25 \%\). In addition, CycleTough fittings have been engineered using the latest techniques in Finite Element Analysis (FEA), ensuring problem-free performance for the long haul.

\section*{ADVANTAGES}

\section*{High Impact Strength}

CycleTough systems have a 2:1 safety factor for long-term pressures, and over 3.2:1 for temporary surges. CycleTough systems easily withstand surges over 600 psi .

\section*{Fittings Engineered}

CycleTough fittings are engineered for versatility and reliability. Their unique design features extra material added for reinforcement to withstand the stresses imposed by tough irrigation and forcemain applications.

\section*{Iron Pipe Size Outside Diameter (IPSOD)}

CycleTough systems are made with an IPSOD, which is the same outside diameter configuration as schedule piping and most steel process piping.

\section*{Bottle-tight Joints, Removable Gaskets}

IPEX's patented gasket system not only withstands many times the rated system pressure, but also withstands full vacuum pressures. The unique removable gasket system allows special oil-resistant (nitrile) gaskets to be easily installed when working in contaminated soils.

\section*{Third-party Certification}

All CycleTough systems are certified to CSA B137.3. Third-party certification verifies a system will perform as expected, meeting all applicable standards```


[^0]:    * Pressure class includes a 2:5:1 safety factor and a $2 \mathrm{ft} / \mathrm{s}$ surge allowance.

[^1]:    ${ }^{2}$ Hulsmann, Nowack,"70 Years of Experience with PVC Pipes" Conference Paper, Plastic Pipes XII, Milan, April 2004

[^2]:    *Values have been rounded to the nearest 5 psi

[^3]:    ${ }^{6}$ Uni-Bell PVC Pipe Association, "Handbook of PVC Pipe - Design and Construction", fourth edition, (August 2001)

[^4]:    ${ }_{8}^{7}$ AWWA Manual M23, $2^{\text {nd }}$ Edition - PVC Pipe - Design and Installation, 2002, American Water Works Association
    8 "Pump Handbook - Third Edition" - Karassik, messina, Cooper \& Heald, pp.8.36

